

CALDWELL MARINE INTERNATIONAL TECHNICAL PROPOSAL

POSEIDON DC PROJECT TYPICAL SUBMARINE CABLE INSTALLATION





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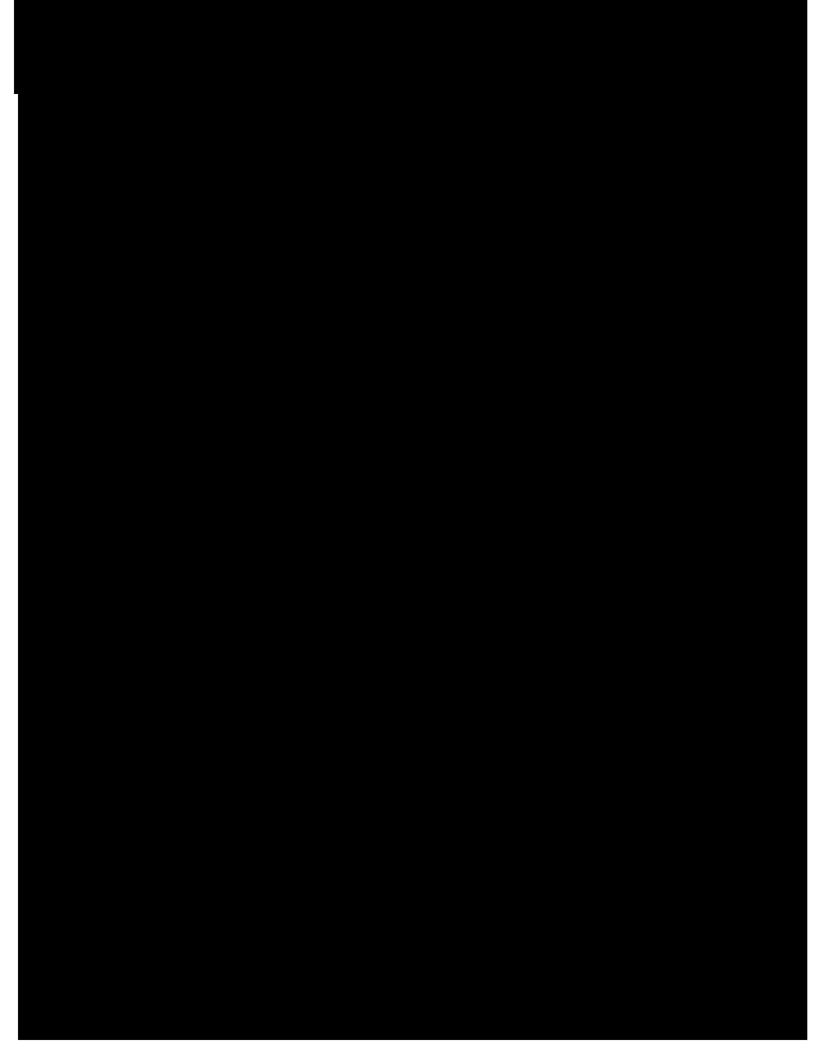


1 Introduction

Caldwell Marine International is pleased to provide the following preliminary generic proposal for the installation of the HVDC submarine cable circuit, in support of the Poseidon Cable Project. As always, we look forward to providing marine support services for this and all future projects. Based upon our 50 years of marine construction and submarine cable experience Caldwell Marine International can provide a highly effective team of professionals experienced with all aspects of submarine cable operations. In addition to our experienced personnel, Caldwell Marine International maintains an impressive array of specialized cable handling equipment, cable embedment plows, cable and cable support vessels, and marine facilities.

Caldwell Marine International shall follow the procedure guidelines set forth in this proposal. All work shall be performed in a safe and expedient manner. **No work is so important that safety becomes a secondary issue.**

A project specific Method Description can be submitted upon receipt of all information required to complete a firm proposal.



ANBARIC DEVELOPMENT PARTNERS

AC and DC Land & Submarine Transmission Cable EMF Study

Revision A

Project number: 154482

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EMF STUDY

PREPARED FOR:

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"Issued For" Definitions:

- "Prelim" means this document is issued for preliminary review, not for implementation
- "Appvl" means this document is issued for review and approval, not for implementation
- "Impl" means this document is issued for implementation
- "Record" means this document is issued after project completion for project file

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1.0 EXECUTIVE SUMMARY

POWER Engineer Consulting (POWER) has been contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform an Electric and Magnetic Field (EMF) study on the contracted by Anbaric Development Partners to perform the contracted by Anbaric Development Partners to perform the contracted by A

EMF effects were calculated for five cases in Safe Engineering Service's Current Distribution, Electromagnetic Interference, Grounding and Soil Structure Analysis (CDEGS) HIFREQ software. Separate simulations were created for AC and DC. One simulation was performed for the 1,200 MW AC cable system and one simulation at 320kV and 400kV for each 1,200MW DC cable system. EMF coupling interaction between the HVDC and HVAC cables was not analyzed. The characteristics of the cables can be seen in Appendix A. All cables were considered to be in-service for both AC and DC systems for this investigation. AC configurations will be cross-phased (ABC-CBA top to bottom) to minimize EMF effects. Table 1 shows the maximum magnetic field calculation results for each cable:

	Table 1: Magnetic Field Results	
Cable Type	Nominal Voltage (KV)*	Maximum Magnetic Field (mG)
DC Underground	320kV	468.05
DC Underground	400kV	347.44
DC Submarine	320kV	711.35
DC Submarine	400kV	569.07
AC Underground	345kV	37.76

The results section includes plots which indicate the magnetic fields for each of the DC and AC systems. The results for the electric fields above ground were negligible and not included in this report. All the transmission systems are within recommended guidelines and standard (shown in Section 2.2).

2.0 ANALYSIS

2.1 Objectives

The objective of this study was to provide analysis of the EMF values for a specific segment of the that is being installed and report the results for one meter above grade. The calculated EMF values are compared against the New York Public Service Commission (NYPSC) and the International Commission on Non-Ionizing Radiation Protection (ICNIRP) limits to provide a point of comparison.

2.2 EMF

The EMF analyses are performed using Safe Engineering Service's Current Distribution, Electromagnetic Interference, Grounding and Soil Structure Analysis (CDEGS) HIFREQ software. HIFREQ uses the electrical and physical characteristics of the transmission line to calculate EMF from the transmission lines.

The electric fields are primarily a function of the maximum operating voltage of conductors. Magnetic fields are primarily a function of the line current loading, which varies over time. Therefore, the magnetic fields calculations are performed at calculated maximum line current loading.

For the analysis, electric and magnetic fields were analyzed one meter above grade with the AC cable depths based on the plan and profile drawings, see Appendix B, and the DC cable depths were at analyzed at three feet for land and fourteen feet for submarine. The distance between the DC cables is twenty inches for underground and thirty-three feet for submarine. In this analysis, all cables are considered to be in-service.

Once EMF values are calculated, they are compared to recommended guidelines and standards as shown in the results section. The New York Public Service Commission (NYPSC) provides a limit for electric fields of 1.6 kV/m, and a limit for magnetic fields of 200 mG, both at the edge of the ROW for AC transmission systems. The data is per the Statement of Interim Policy on Magnetic Fields of Major Electric Transmission Facilities issued September 11, 1990. The International Commission on Non-Ionizing Radiation Protection (ICNIRP) provides a limit for electric fields at 8.33kV/m, and a limit of 400mT (4 million mG) for magnetic fields on DC transmission systems. The data is per the ICNIRP published in 1998.

2.4 Input Data

Electric and magnetic field performance is all based on the electrical and physical characteristics of the transmission lines. Specifically, these factors are driven by the voltage and current loading of the line, the physical conductor characteristics bundling, and the relationships of each phase conductor to the other phases. As a result, there are several variables that will affect calculated results. These conductors were modeled without the outer shield of the cables grounded as it yields the worst-case results. Should any of the cable or design data change, the results will also change.

3.0 EMF RESULTS

3.1 Magnetic Fields

The reported magnetic field values are the maximum magnetic flux densities at a given point in space. Magnetic flux density is in units of gauss or milligauss (mG). The NYPSC limits the magnetic field to 200 mG at the edge of the ROW for AC transmission systems and the ICNIRP limits the magnetic field to 400mT (4 million mG) at the edge of the ROW for DC transmission systems. Table 2 shows the maximum magnetic fields for the AC and DC underground transmission systems.

	Table 2: Magnetic Field Results	
Cable Type	Nominal Voltage (KV)*	Maximum Magnetic Field (mG)
DC Underground	320kV	468.05
DC Underground	400kV	347.44
DC Submarine	320kV	711.35
DC Submarine	400kV	569.07
AC Underground	345kV	37.76

The calculated edge of ROW magnetic fields are within the recommended guidelines and standards limits.

The following figures show the calculated magnetic fields within the ROW:

- Figure 1: DC Underground at 320kV
- Figure 2: DC Underground at 400kV
- Figure 3: DC Submarine at 320kV
- Figure 4: DC Submarine 400kV
- Figure 5: AC Underground 345kV

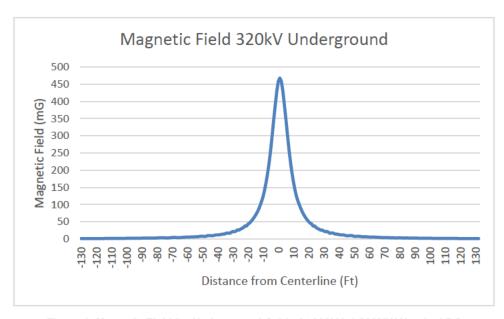


Figure 1: Magnetic Field for Underground Cable At 320kV, 1,200MW Nominal DC

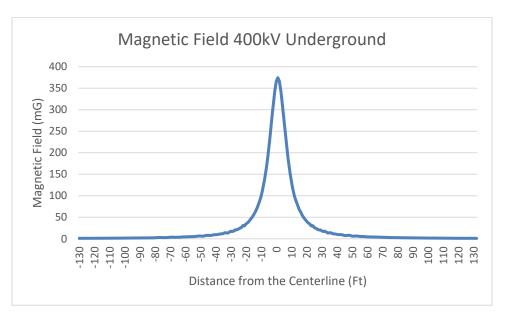


Figure 2: Magnetic Field for Underground Cable At 400kV, 1,200MW Nominal DC

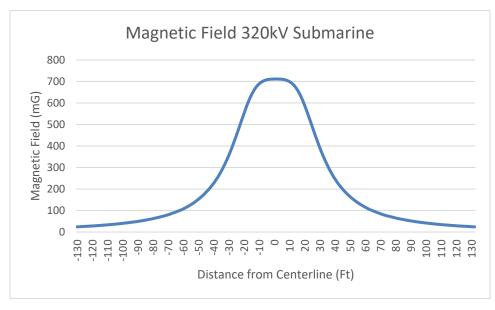


Figure 3: Magnetic Field for Submarine Cable At 320kV, 1,200MW Nominal DC

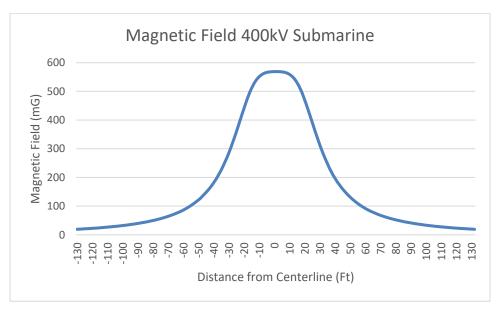


Figure 4: Magnetic Field for Submarine Cable At 400kV, 1,200MW Nominal DC

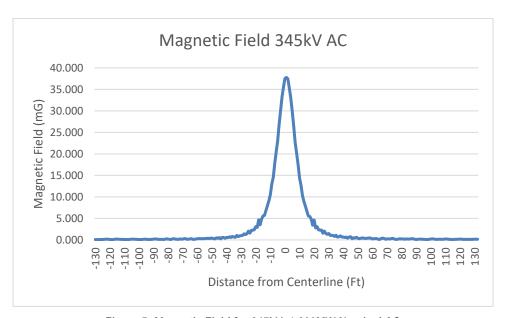


Figure 5: Magnetic Field for 345kV, 1,200MW Nominal AC

4.0 GENERAL SUMMARY OF RESULTS

The calculated EMF effect results for the follows:

- The calculated magnetic field for the DC system is below the limit of 4 million mG.
- The calculated magnetic field for the AC system is below the limit of 200mG
- Electric fields above ground from the underground transmission lines are negligible.



Submarine Cable Route Field Evaluations Report

Boardwalk Power Link Project New Jersey State Waters

PREPARED FOR:

Boardwalk Transmission LLC 401 Edgewater Place, Suite 680 Wakefield, MA 01880

PREPARED BY:

ESS Group, Inc. 404 Wyman Street, Suite 375 Waltham, Massachusetts 02451

ESS Project No. A592-003.20

June 2021



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	EA, CONTROL INFORMATION, AND EQUIPMENT



1.0 INTRODUCTION

Boardwalk Powerlink LLC is proposing the Boardwalk Power Link Project (Project), which is a component of the larger proposed New York/New Jersey Ocean Grid Project, which is a proposed offshore subsea electric transmission system designed to transmit renewable energy from offshore wind turbine generators planned to be installed offshore of the New York and New Jersey coasts in Bureau of Ocean Energy Management (BOEM) - authorized Wind Energy Areas (WEA's) and connected to the NY/NJ land-based transmission grid. The planned offshore transmission system is designed to efficiently deliver offshore wind energy generation from its specifically located offshore collector platforms (OCPs) to be located in the Outer Continental Shelf (OCS). These OCP's will serve as the interconnection point between the installed WEA's and this new offshore transmission grid connection to existing electric substations New Jersey and New York.

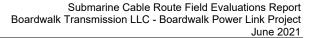
The Boardwalk Power Link Project component, the subject of this report, includes installation (direct seabed burial via jet plow device) of over 33 nautical miles of offshore subsea electric transmission cable from southern New Jersey offshore areas northward in New Jersey waters to Raritan Bay and Keyport Harbor where the subsea cable system will be pulled and installed in an underground transition vault located at the cable's shoreline landfall location.

To obtain route-specific information on the sediment conditions for this alignment, ESS Group, Inc. (ESS) completed sediment sampling field investigations (the "Study") to collect and analyze sediment samples along the Submarine Cable Route, as illustrated in Figure 1. The Study included a sediment sampling program developed to assess sediment bulk physical and chemical properties as well as provide a benthic macroinvertebrate community assessment for seabed sediments along the proposed submarine cable route survey area. The sediment sampling program was preceded by remote-sensing geophysical surveys to acquire hydrography, side-scan sonar, sub-bottom profile, and magnetometer data for the selected survey corridor. The investigation was completed to support associated environmental impact assessments for:

- Environmental regulatory permitting; and
- Preliminary engineering design and installer constructability assessments.

The Sediment Sampling and Analysis Plan (SSAP) to support the overall design of the project and preparation of permit applications was submitted in March 2020 to the New Jersey Department of Environmental Protection (NJDEP). The SSAP was approved by the NJDEP Office of Dredging and Sediment Technology in April 2020 with conditions to run chemical analysis on four locations regardless of grain size composition due to proximity to Historic Area Remediation Site (HARS). The SSAP field work was scheduled to begin in May 2020 but due to Covid-19 restrictions the field work was postponed. The SSAP field work was completed in April 2021. The Project Area was just inside of 3 miles offshore from Sandy Hook New Jersey south to Sea Girt, New Jersey. The sediment sampling performed in April 2021 adds to the previous sampling performed for the Project from 2013-2016.

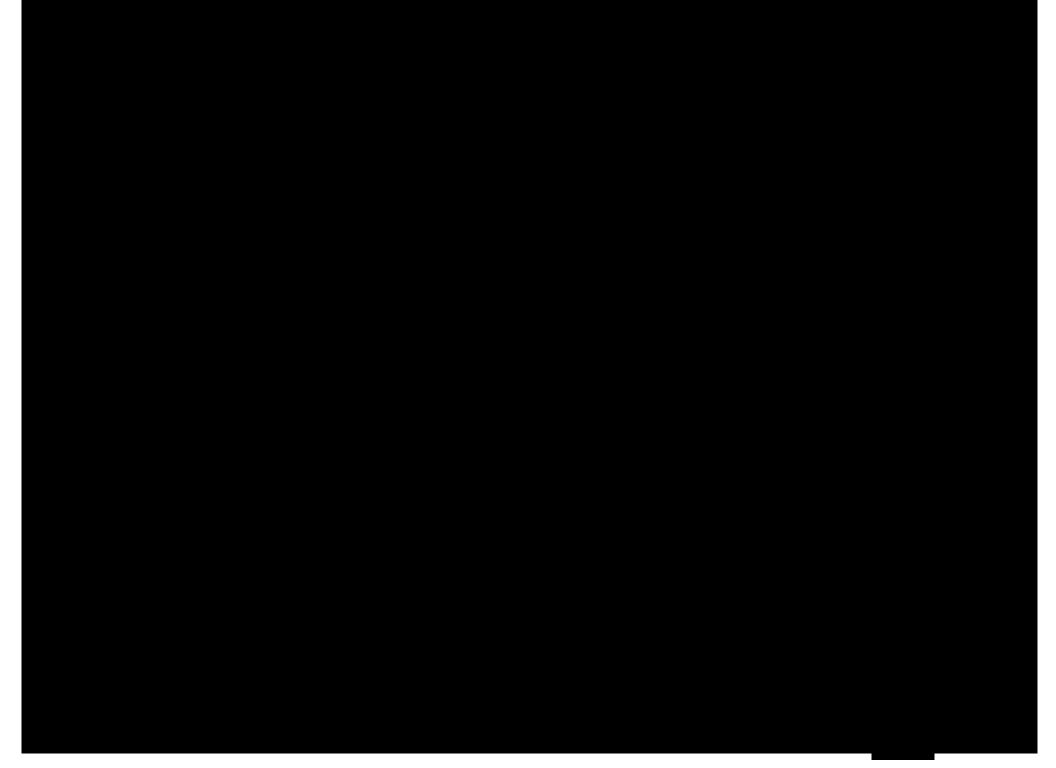
Ocean Surveys Inc. ("OSI") was responsible for field operations (i.e., advancement and collection of vibracores and benthic grabs) and establishing horizontal control. ESS was responsible for directing and observing field activities; splitting, logging, and sampling sediment cores; and coordinating activities with OSI and the analytical laboratories. ESS performed quantitative macroinvertebrate analysis on the benthic samples for evaluation and reporting. OSI contracted the R/V *Connecticut* through the University of Connecticut to support the field program that implemented the SSAP.

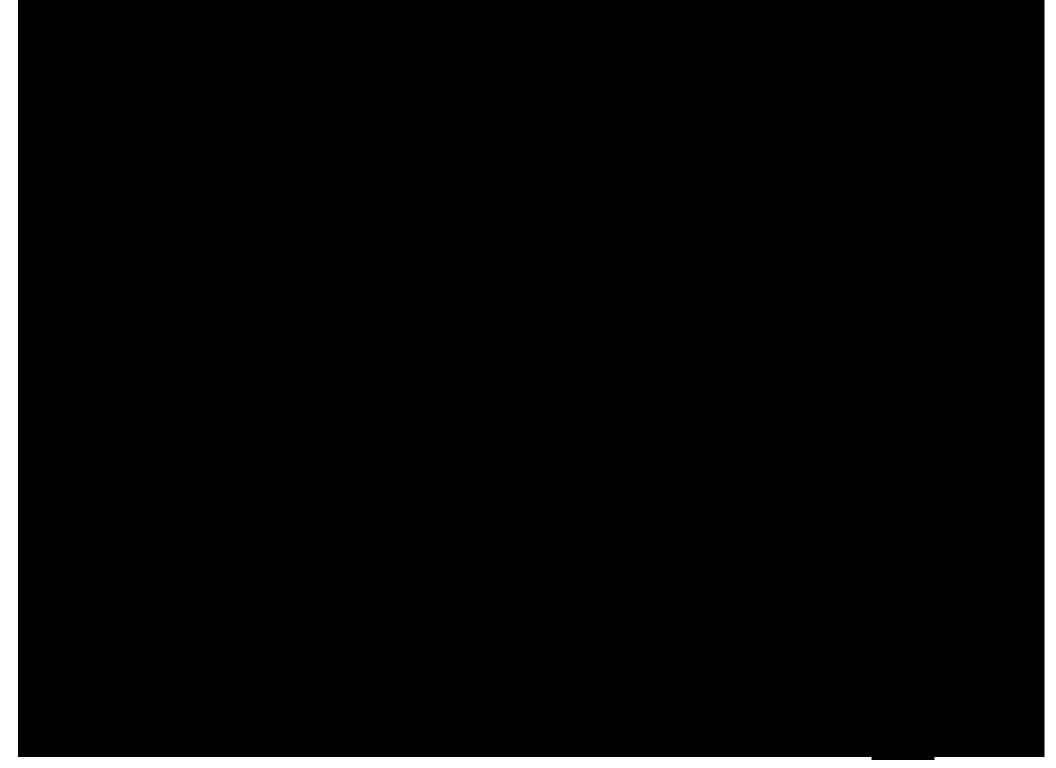


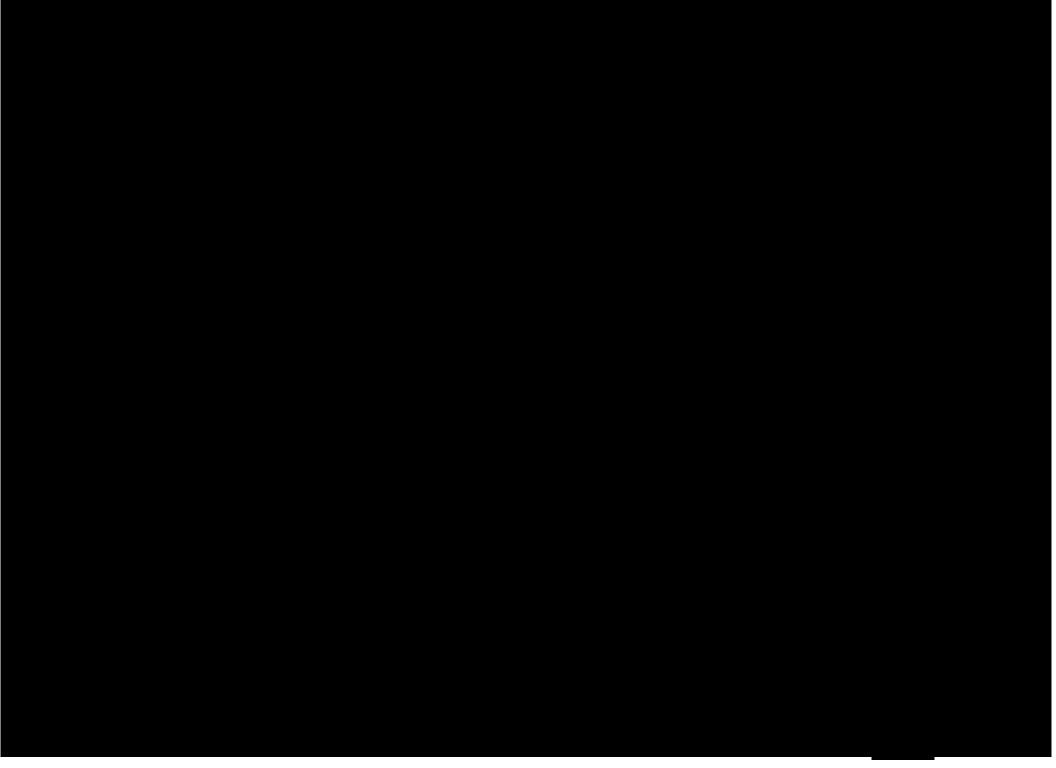
The following sections summarize the methods and findings of the vibracore sediment sampling and analysis portion of the Study. The OSI Operations Report for the field program is provided as Appendix D. A separate ESS report provides the results of the benthic macroinvertebrate sampling is presented in Appendix G.

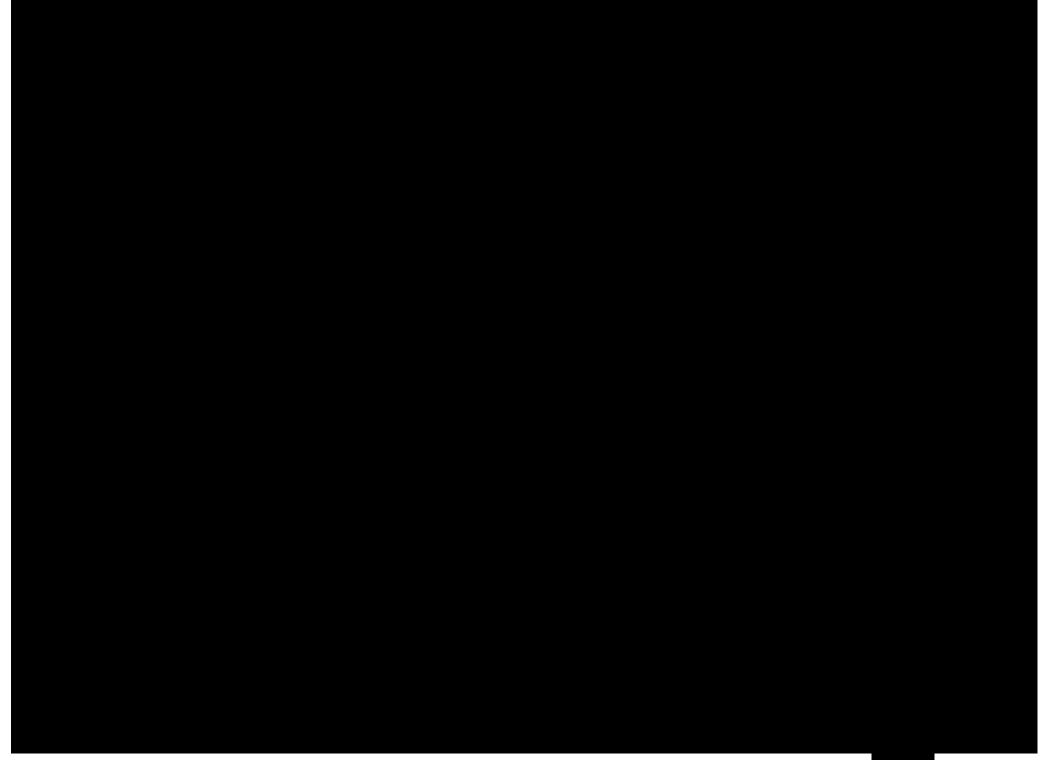


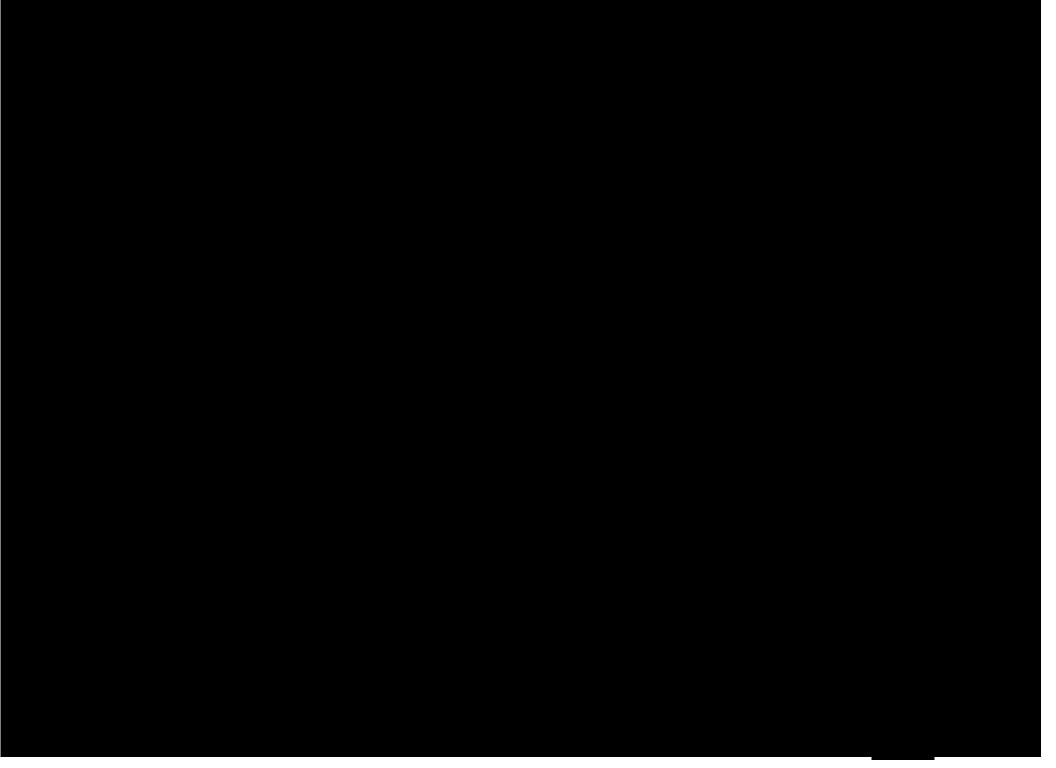


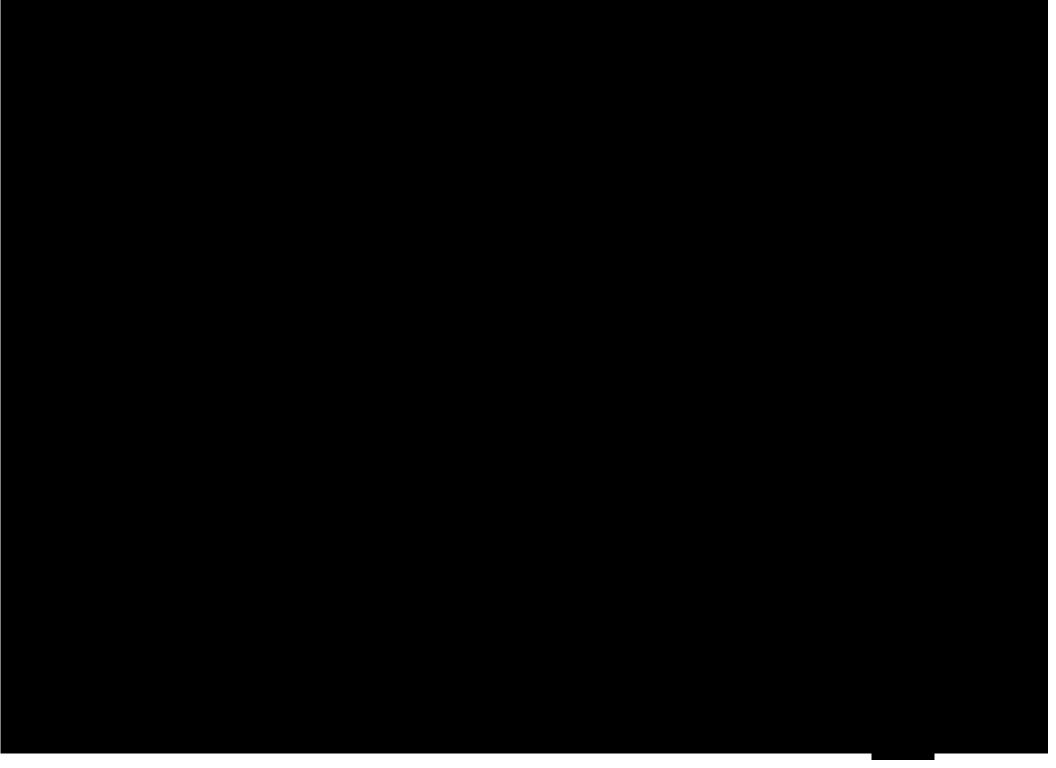


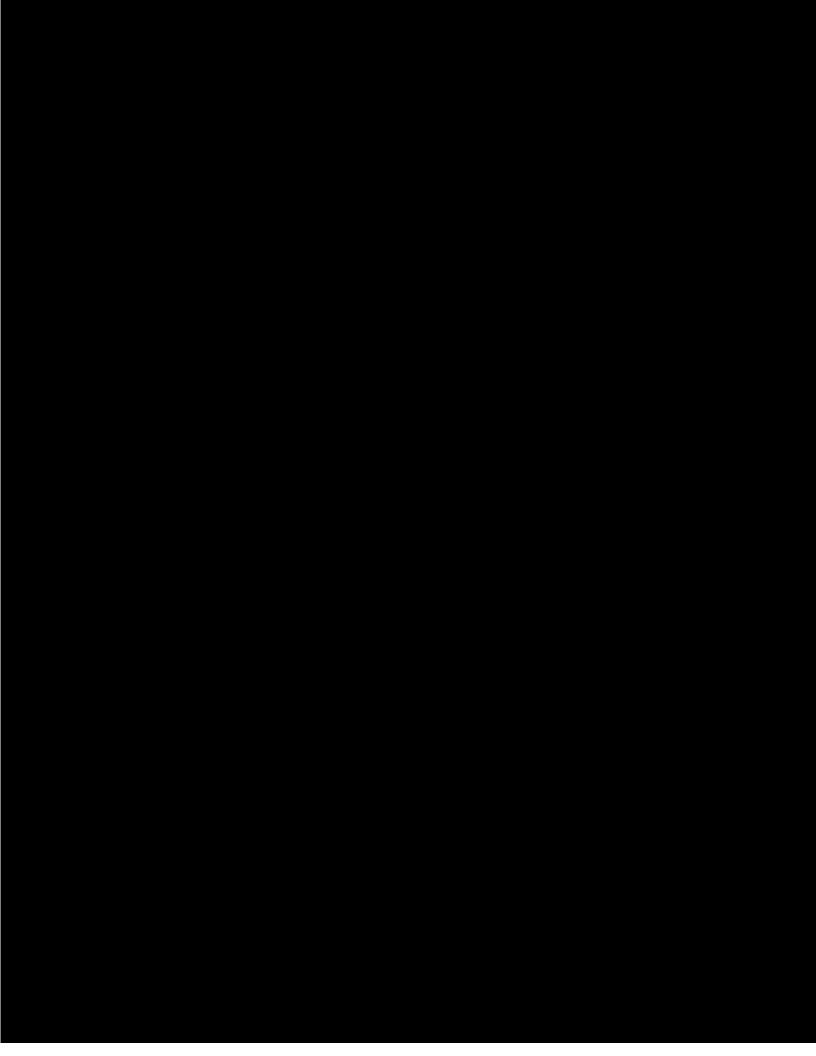


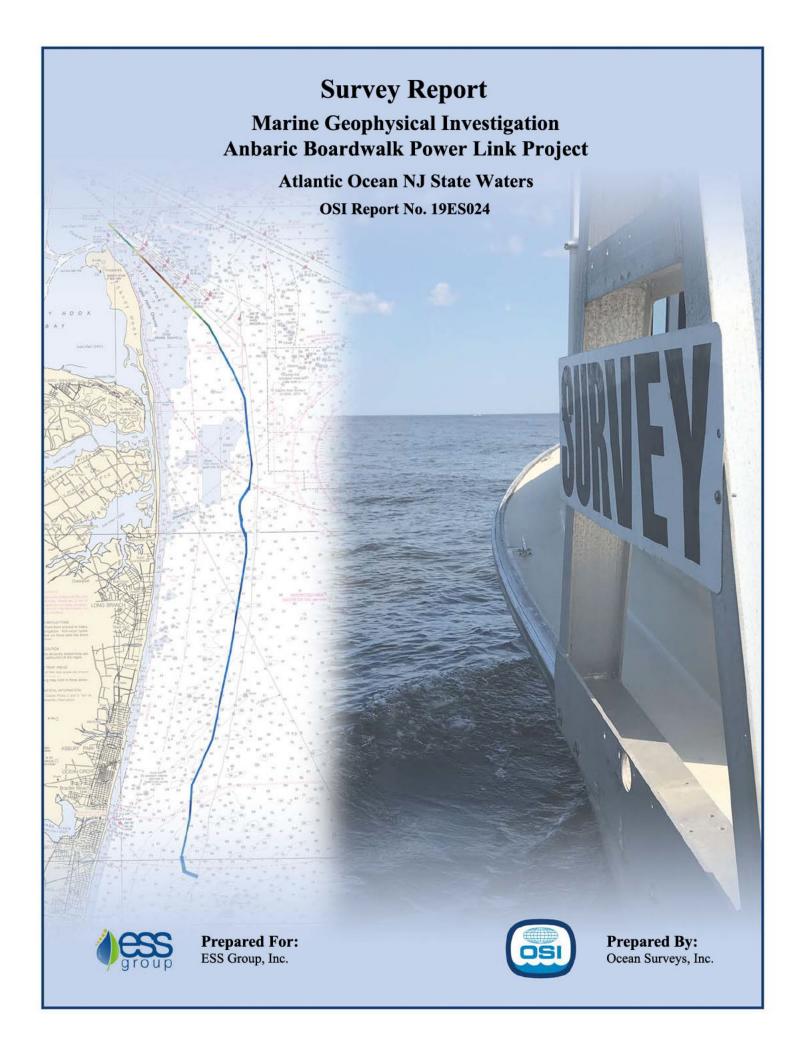












SURVEY REPORT

MARINE GEOPHYSICAL INVESTIGATION ANBARIC BOARDWALK POWER LINK PROJECT ATLANTIC OCEAN NJ STATE WATERS

OSI REPORT NO. 19ES024

Prepared For: ESS Group, Inc.

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East Providence, RI 02915

Prepared By: Ocean Surveys, Inc.

129 Mill Rock Road E. Old Saybrook, CT 06475

Submitted: 12 September 2019 Revised: 15 October 2019

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- 1 Summary Table of Magnetic Anomalies
- Summary Table of Side Scan Sonar Targets &
- Side Scan Sonar Target Reports
- 3 Table of Proposed Vibratory Core Locations
- 4 Reduced Scale Project Drawings (11"by17")

Digital Appendix – Final report and project drawing files, daily client signoff daily field logs, chirp subbottom profiles (jpg format) and a survey trackline log (PDF format).

John D. Sullivan, P.G.

Manager Geophysical Surveys

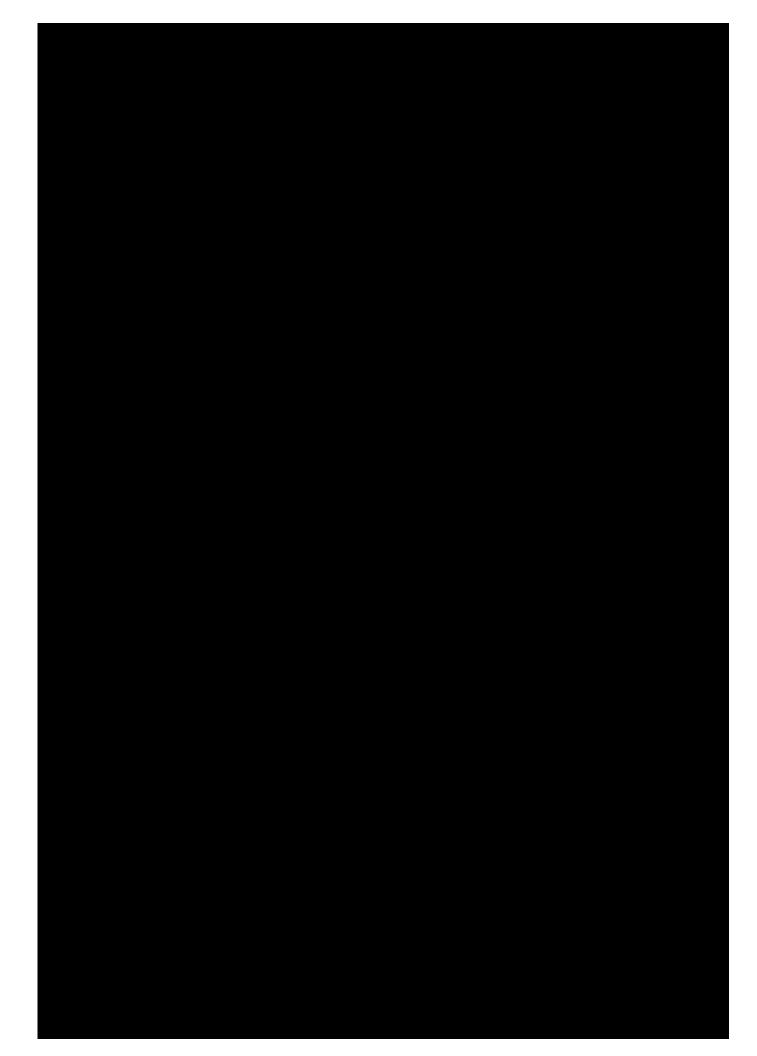
OCEAN SURVEYS, INC.

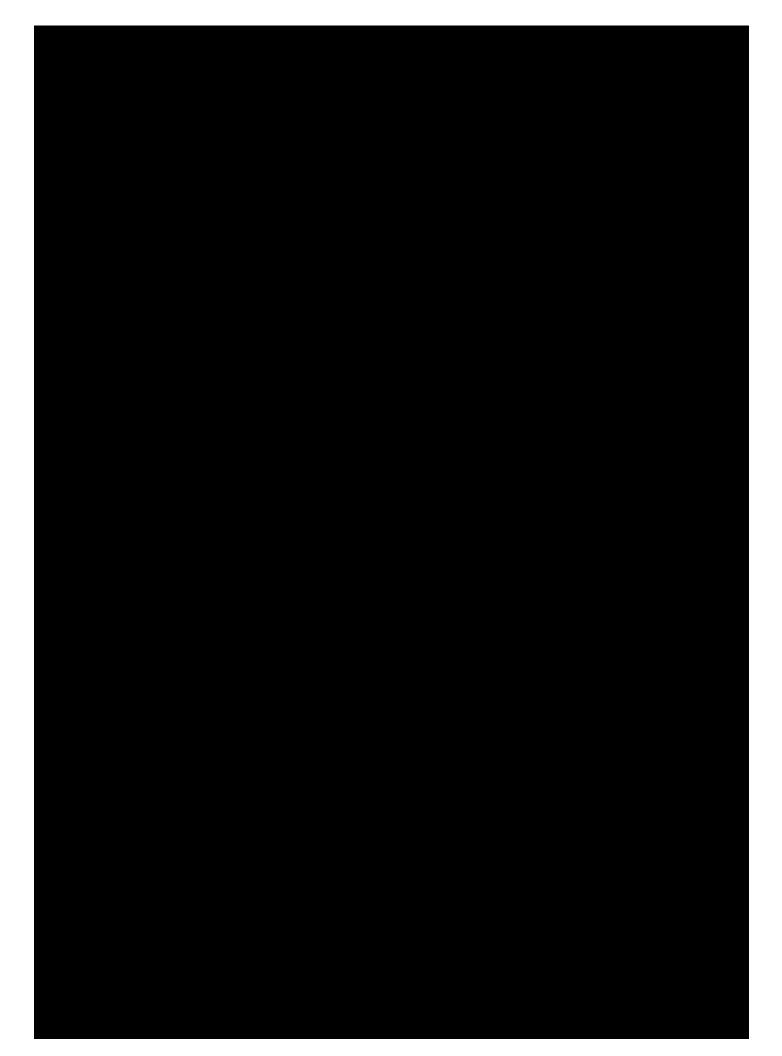
SURVEY REPORT

MARINE GEOPHYSICAL INVESTIGATION ANBARIC BOARDWALK POWER LINK PROJECT ATLANTIC OCEAN NJ STATE WATERS

1.0 INTRODUCTION

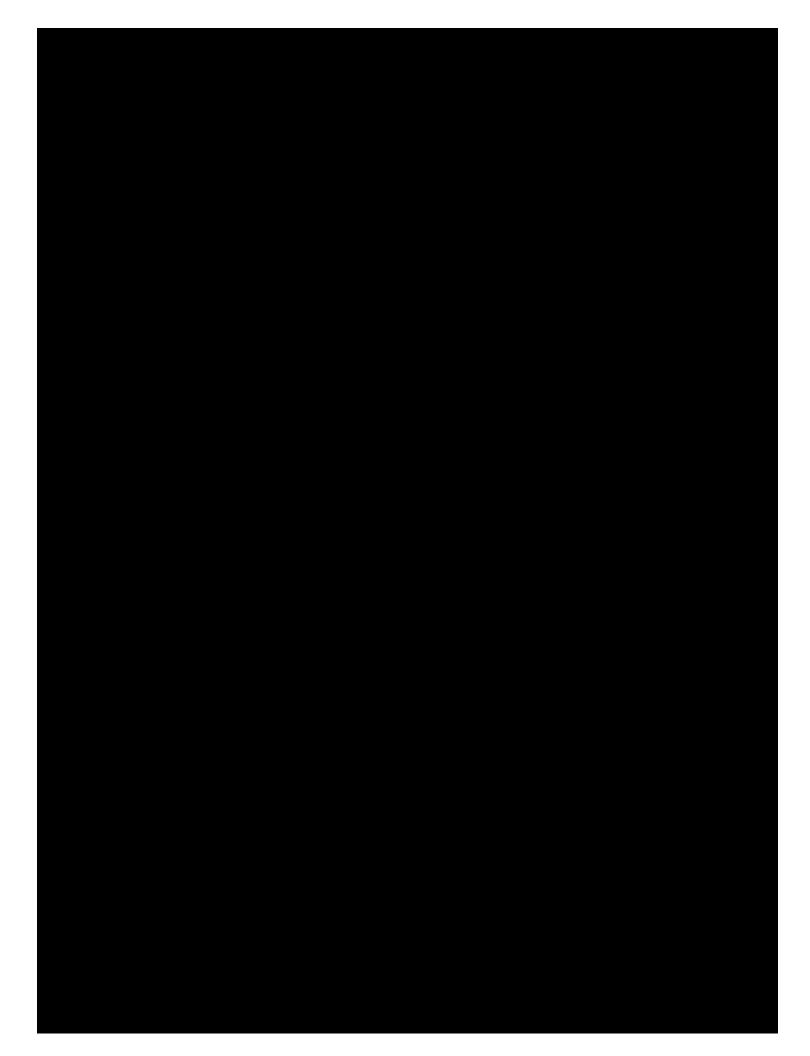
During the period 19-29 July 2019, Ocean Surveys, Inc. (OSI) performed a multi-sensor marine geophysical survey in the Atlantic Ocean offshore New Jersey (NJ). This survey was completed under subcontract to ESS Group, Inc. (ESS) for the Anbaric Development Partners (ADP) to support the development and permitting of a proposed submarine transmission system which will provide a means to interconnect future offshore wind energy generation projects to the onshore electric grid in NJ. The proposed transmission system, referred to as the Boardwalk Power Link Project (Boardwalk), will tie-into a previously investigated transmission project offshore Sandy Hook NJ, run south in NJ state waters and provide a means to interconnect to projects in federal waters offshore of New Jersey (Figure 1). Future planned investigations will include a geotechnical sampling program to ground-truth the geophysical interpretation presented herein and to assist in permitting the Project.







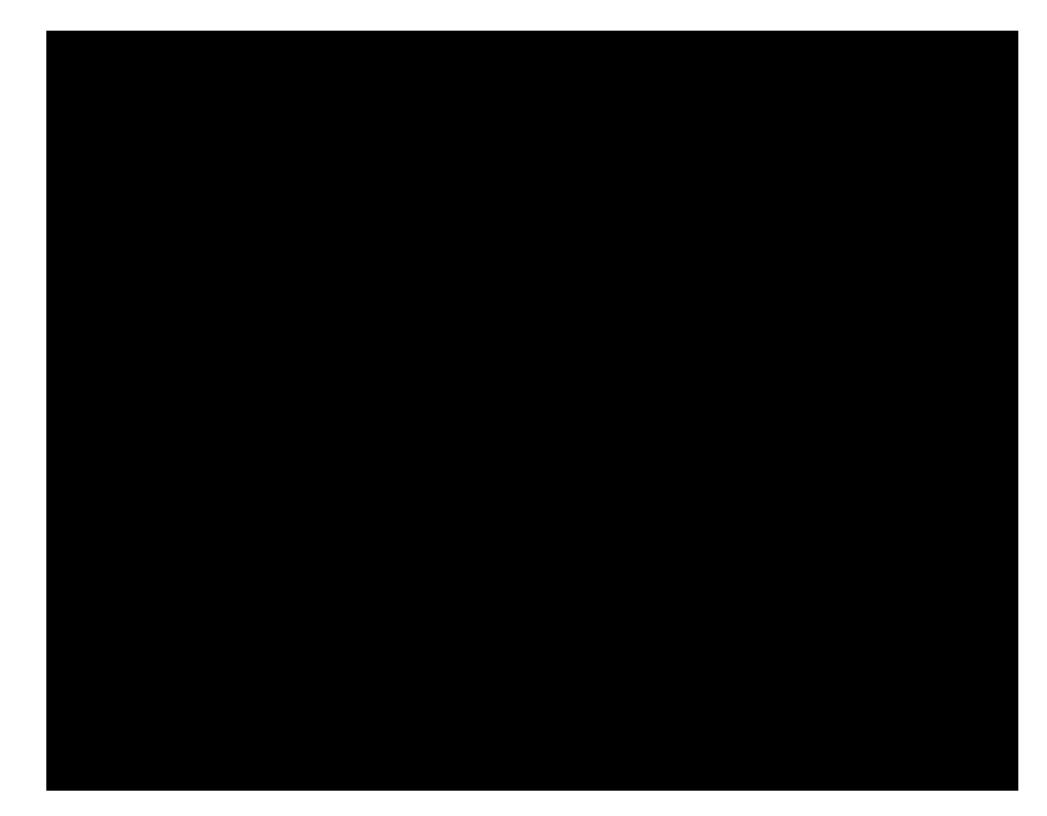














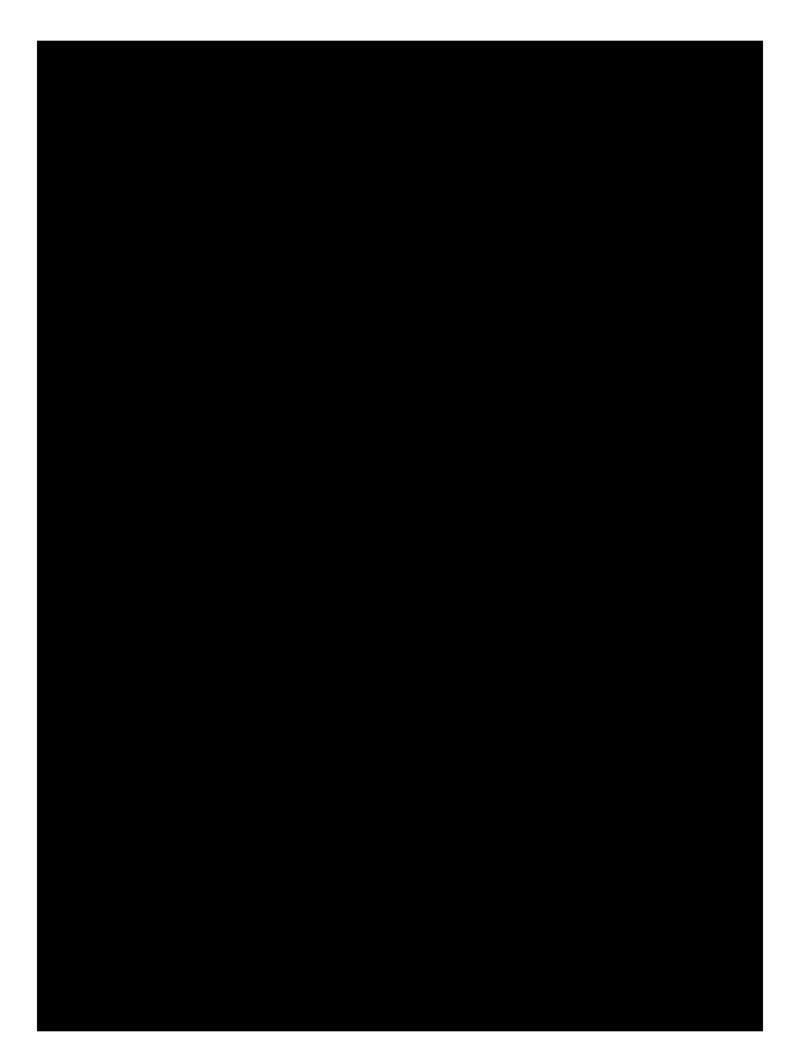


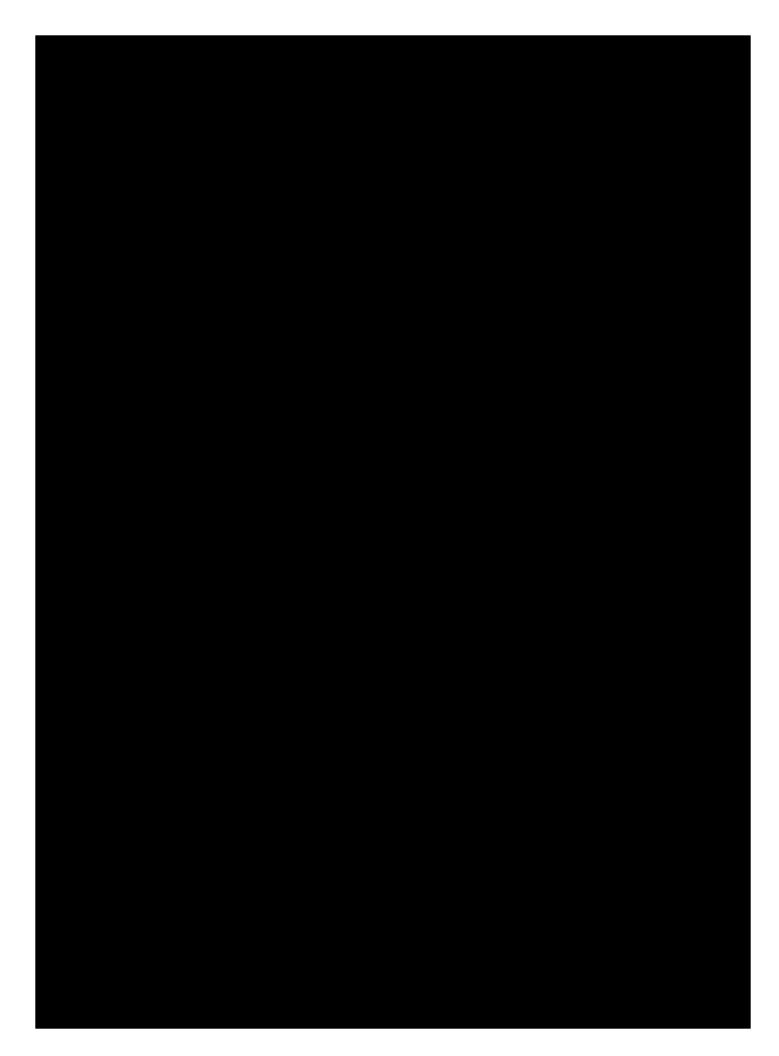








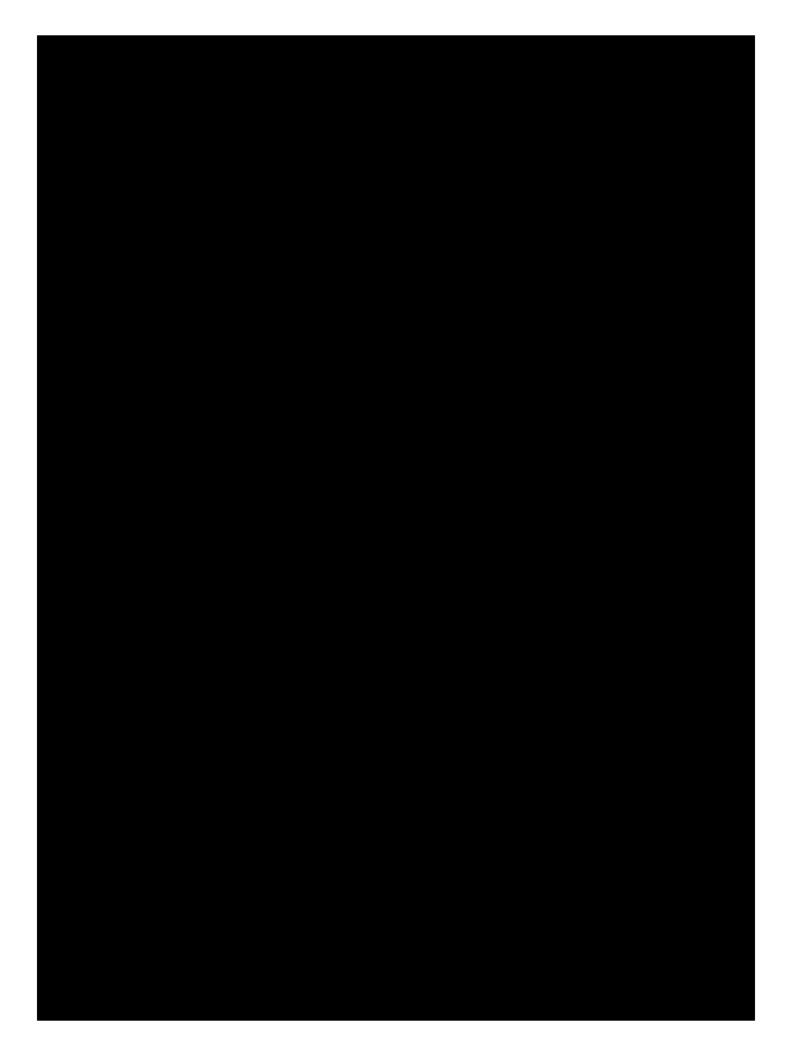


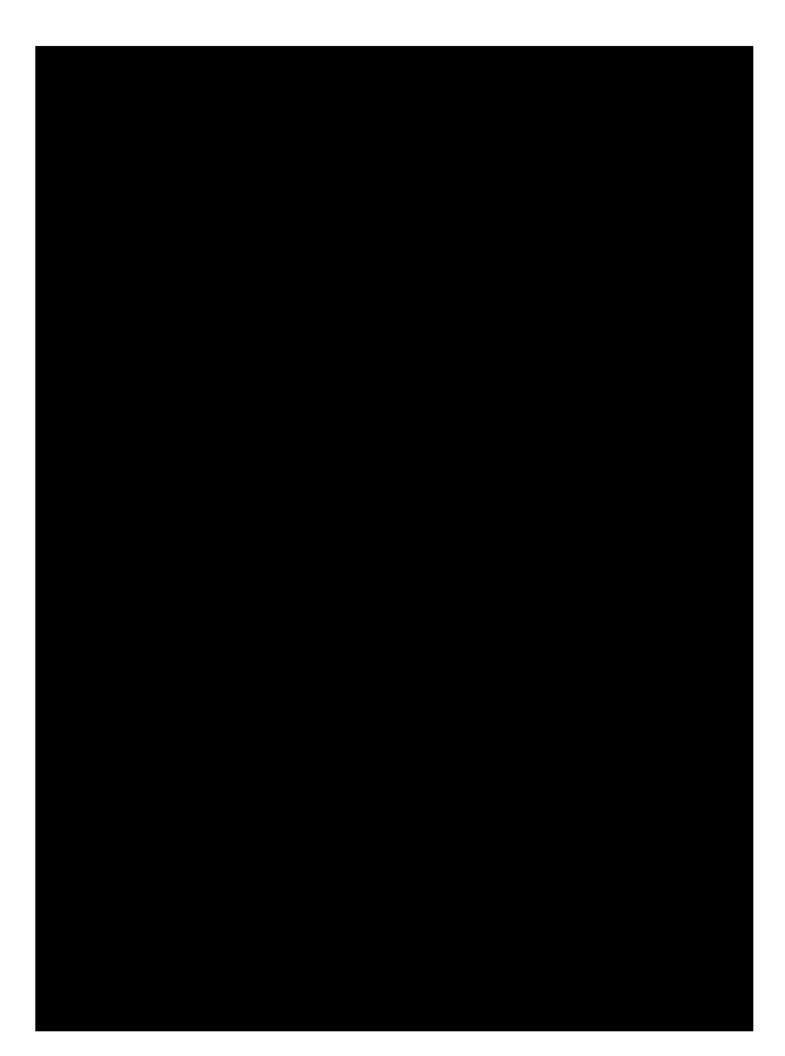




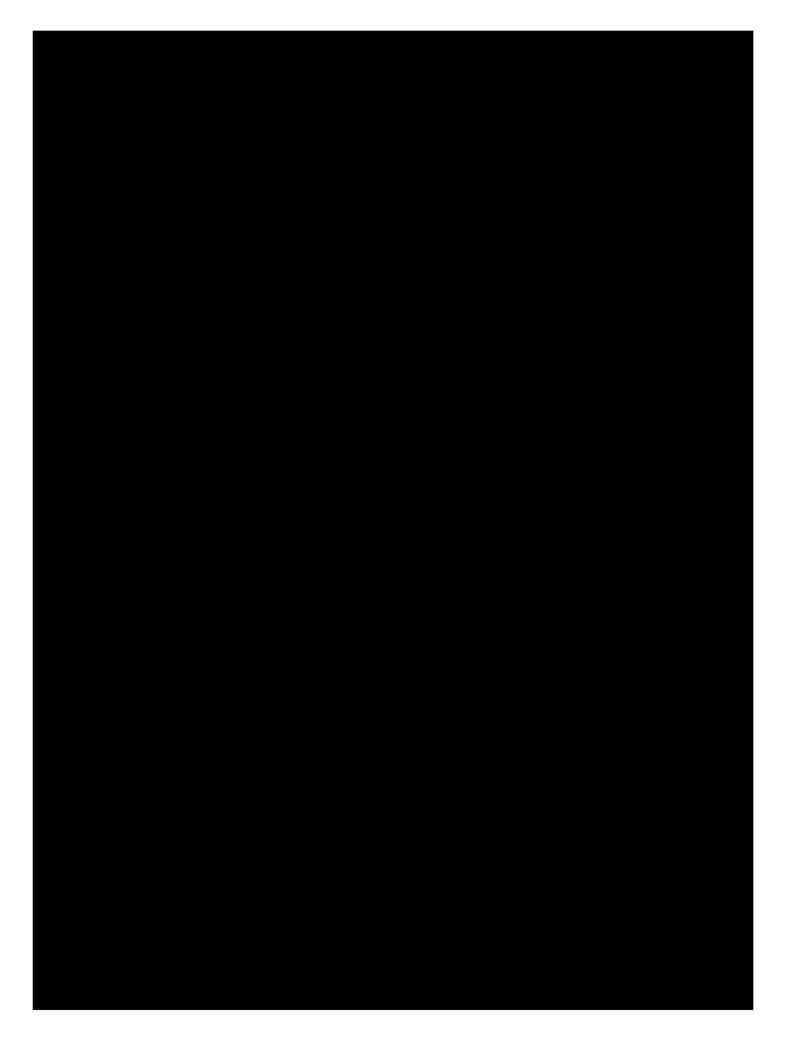






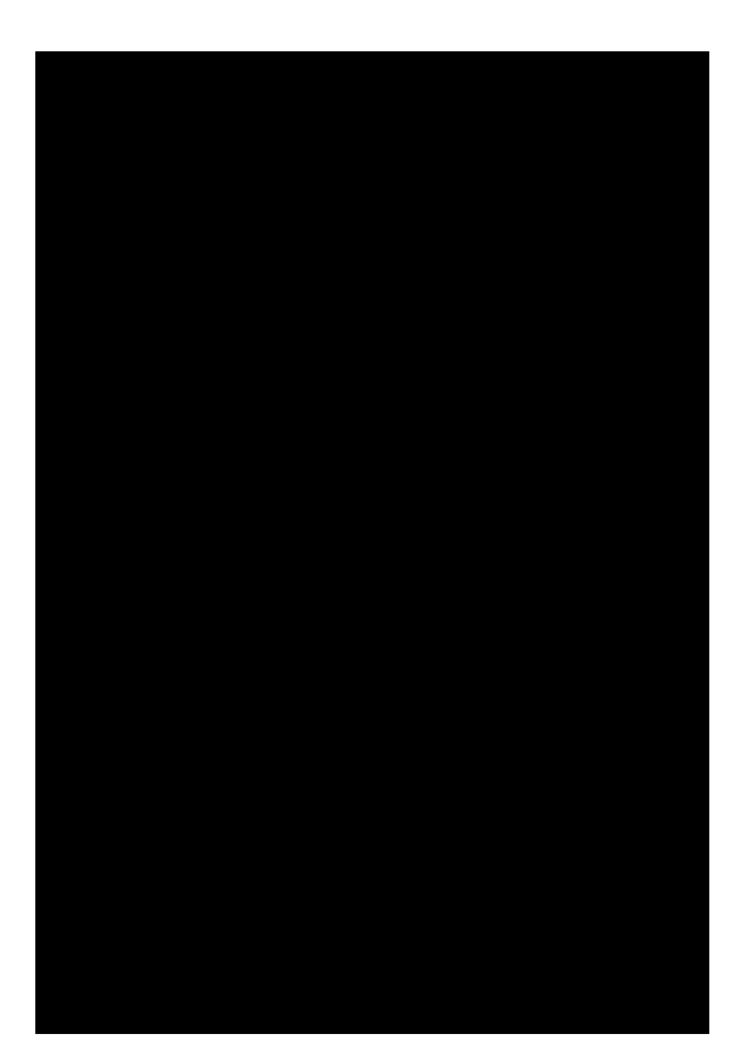


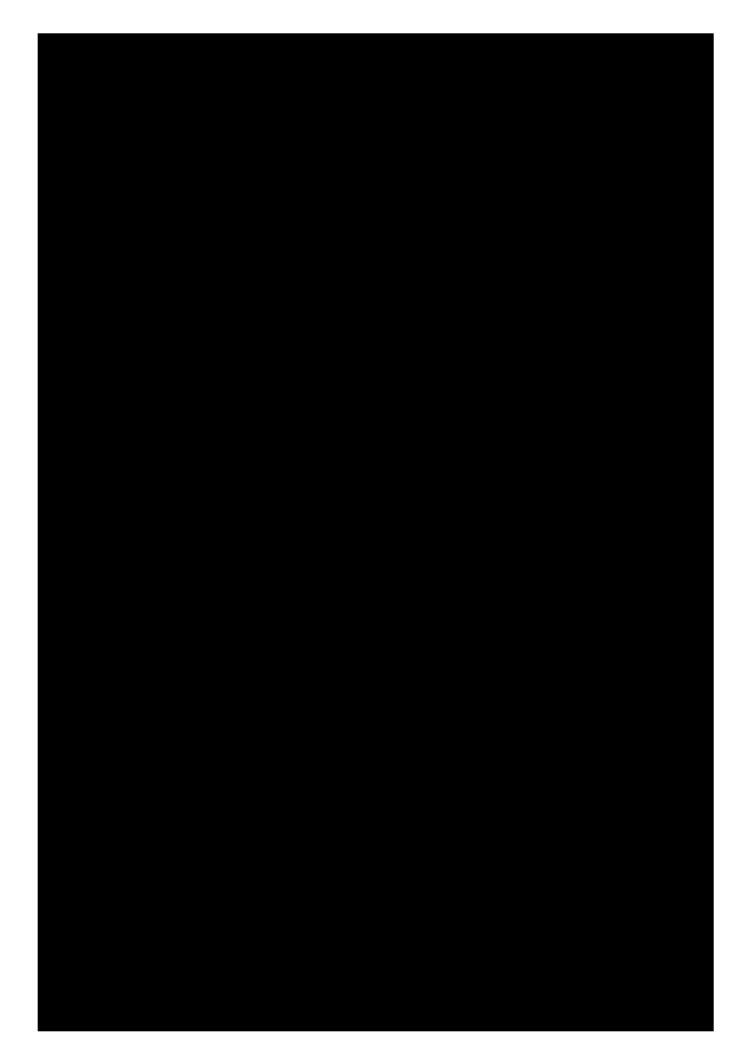




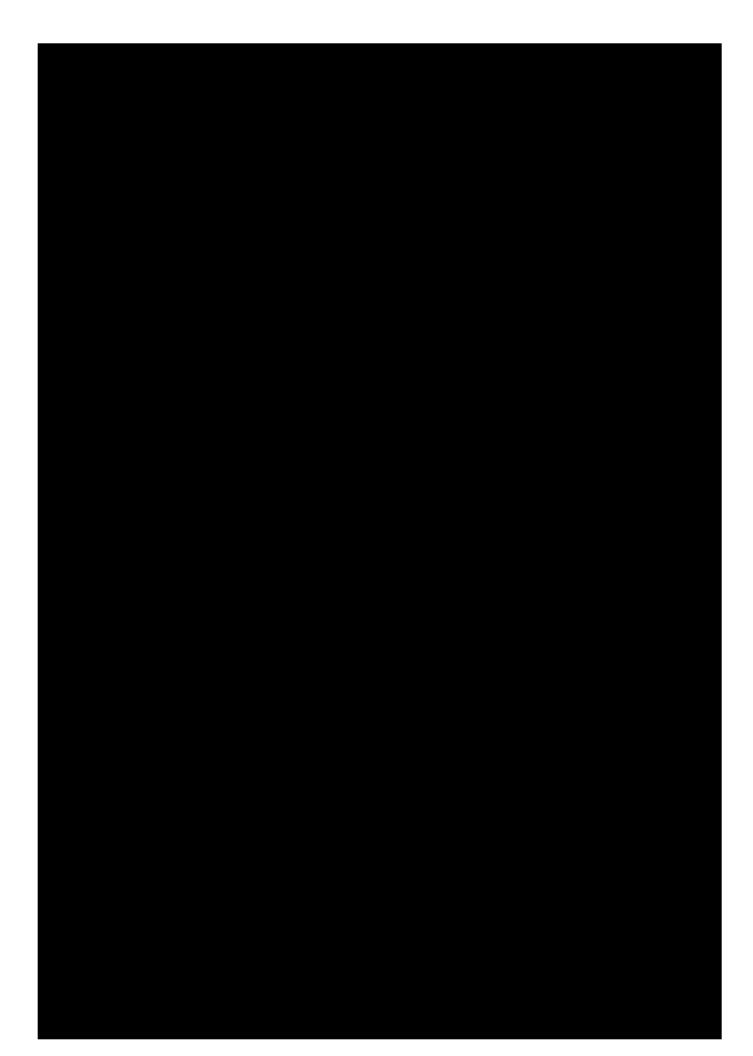


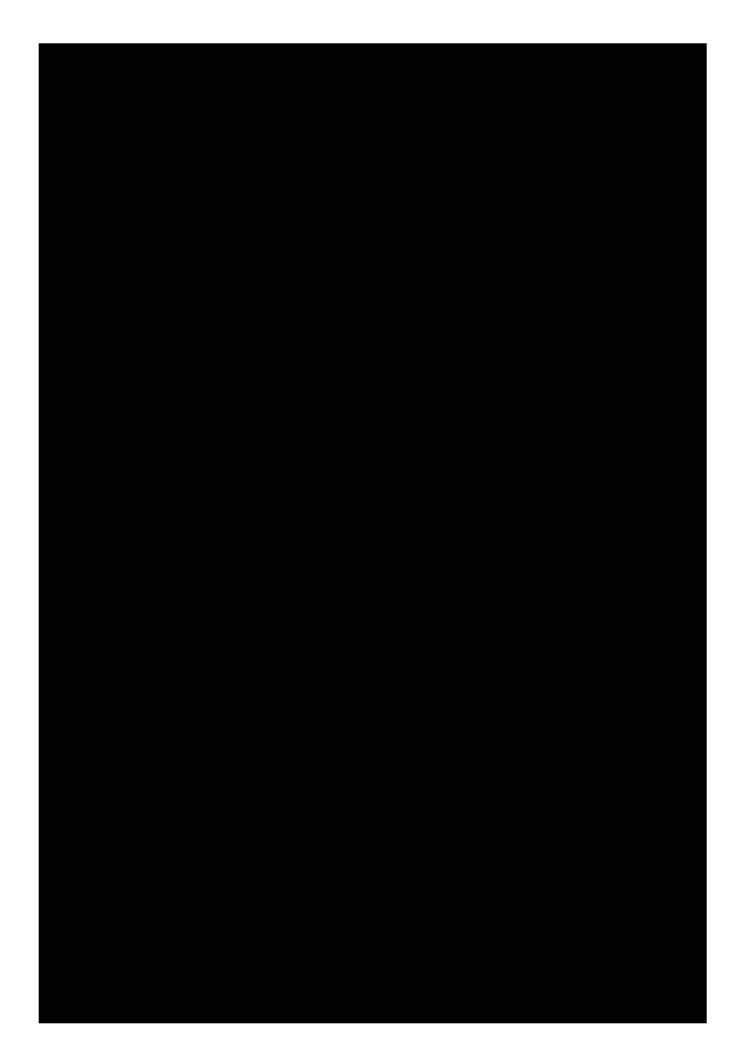


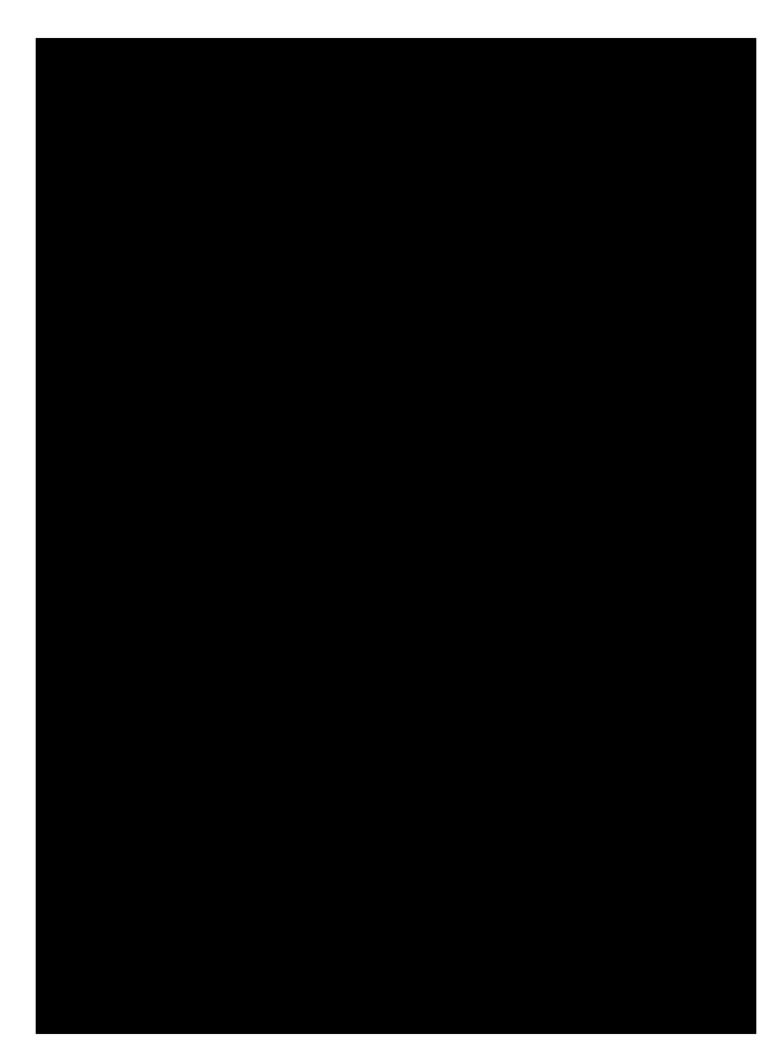






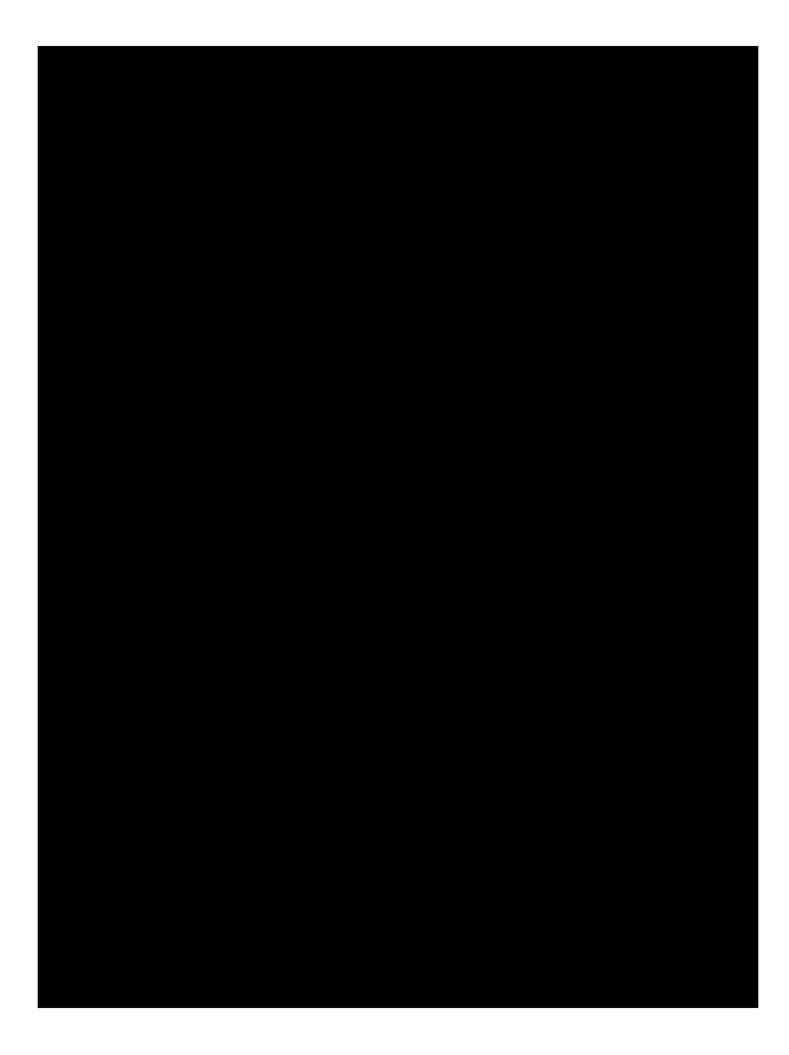


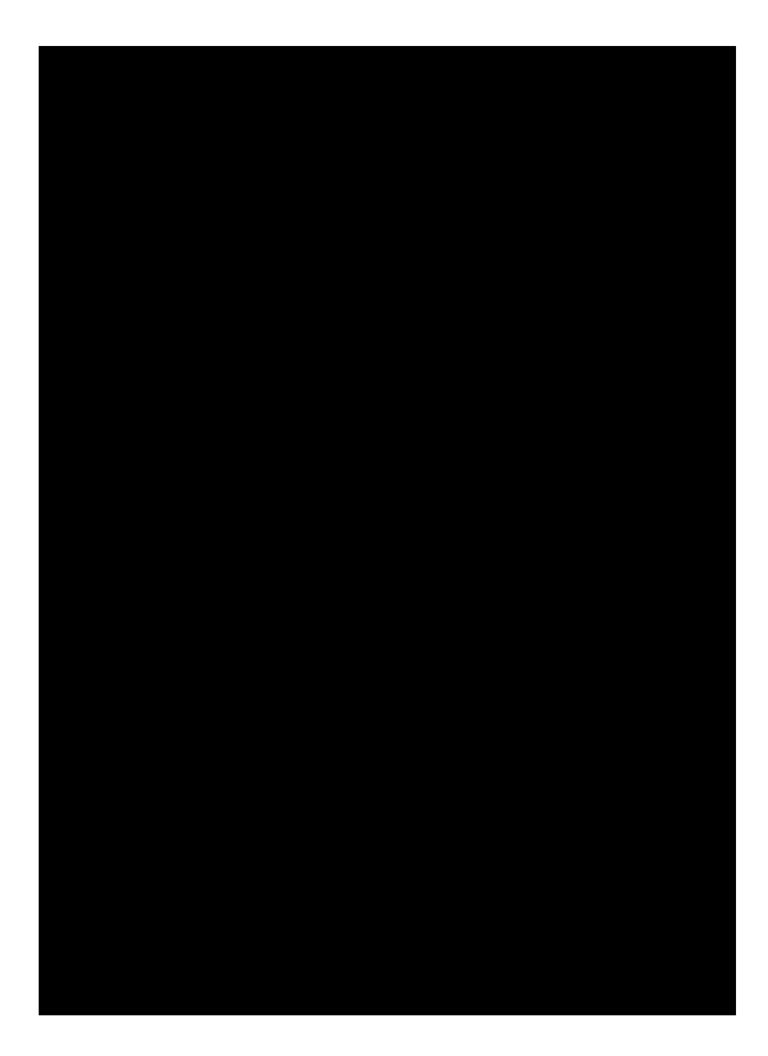




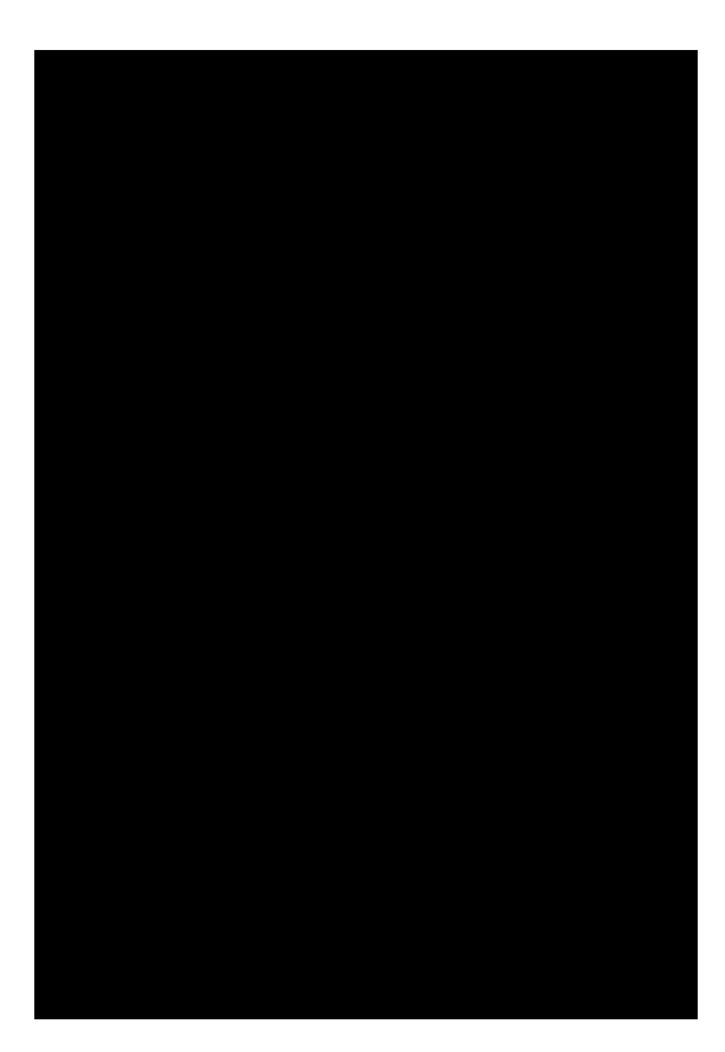


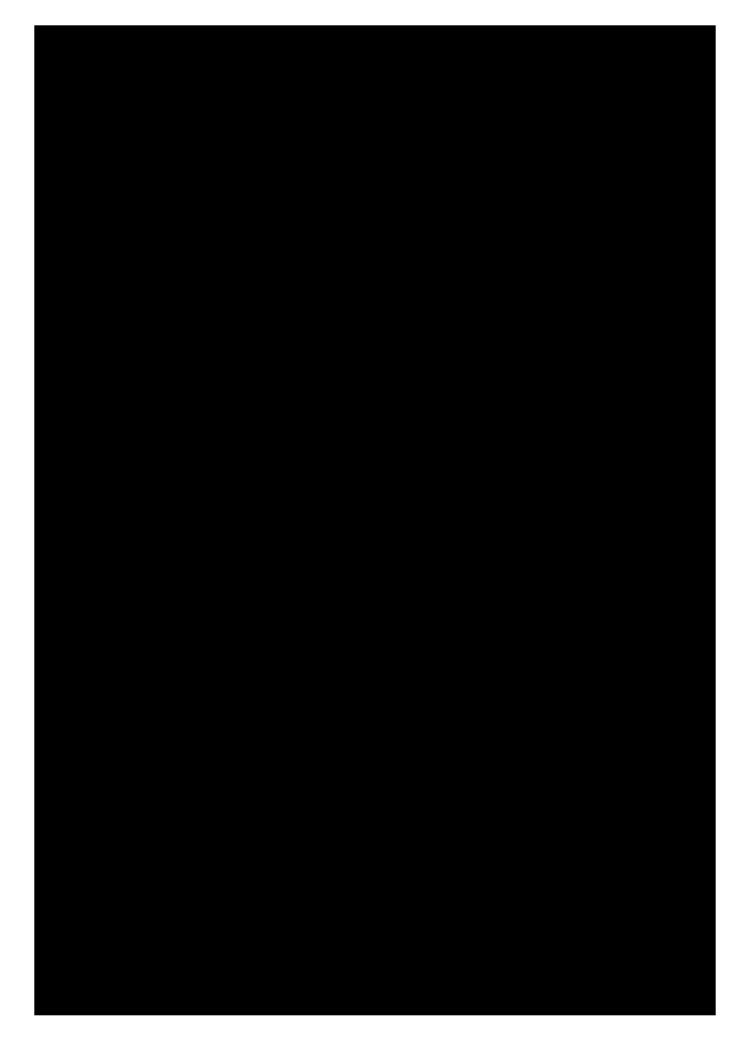






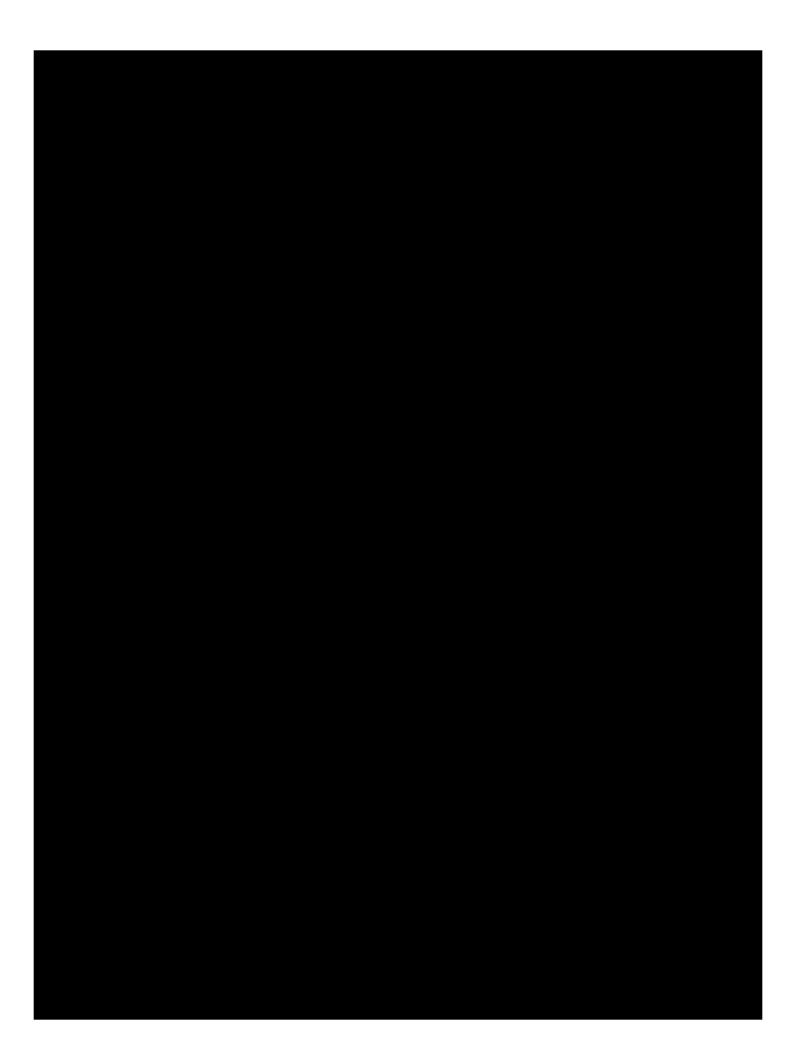


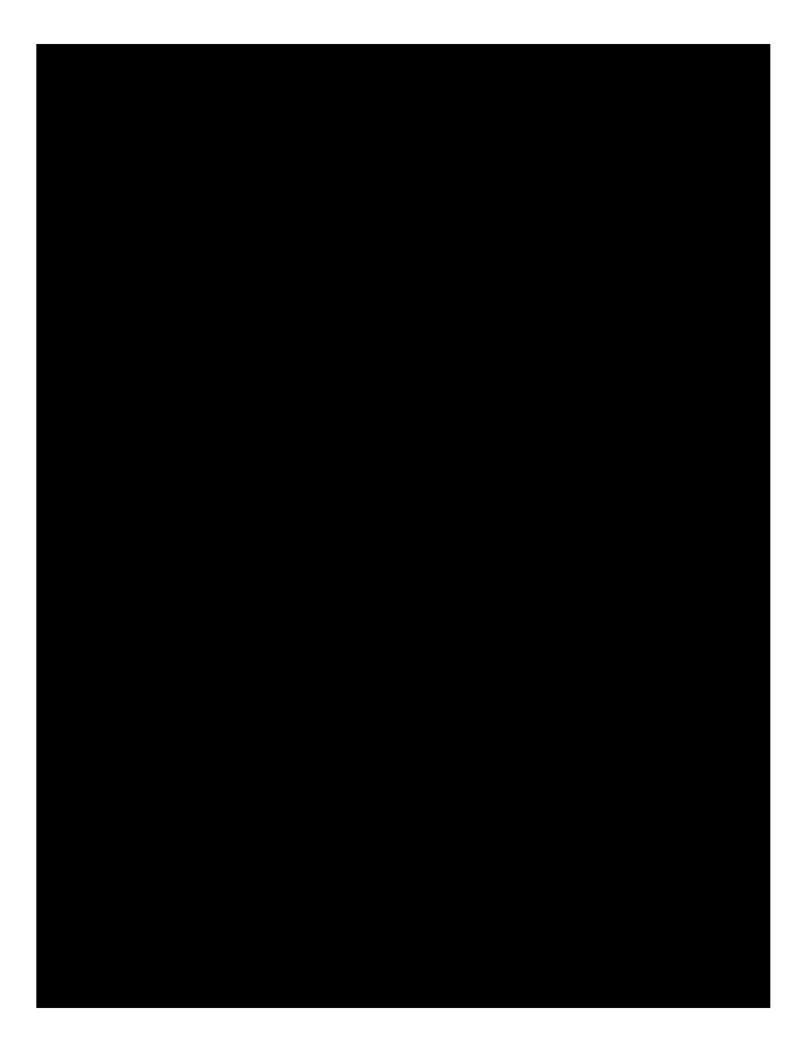




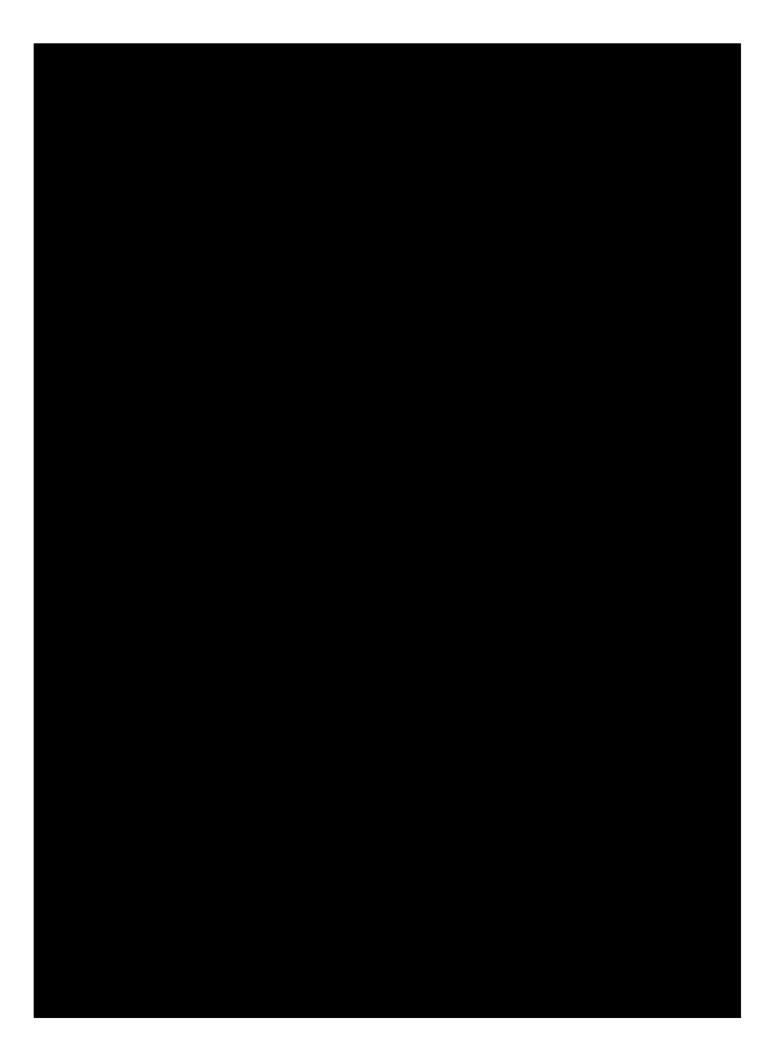


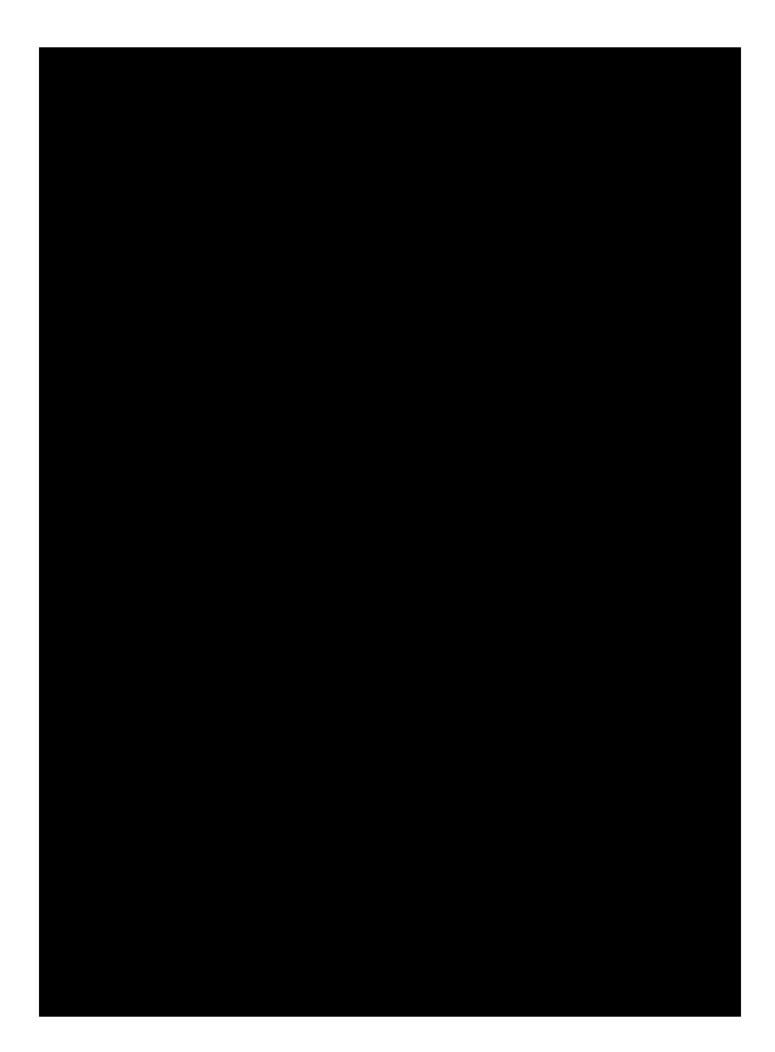










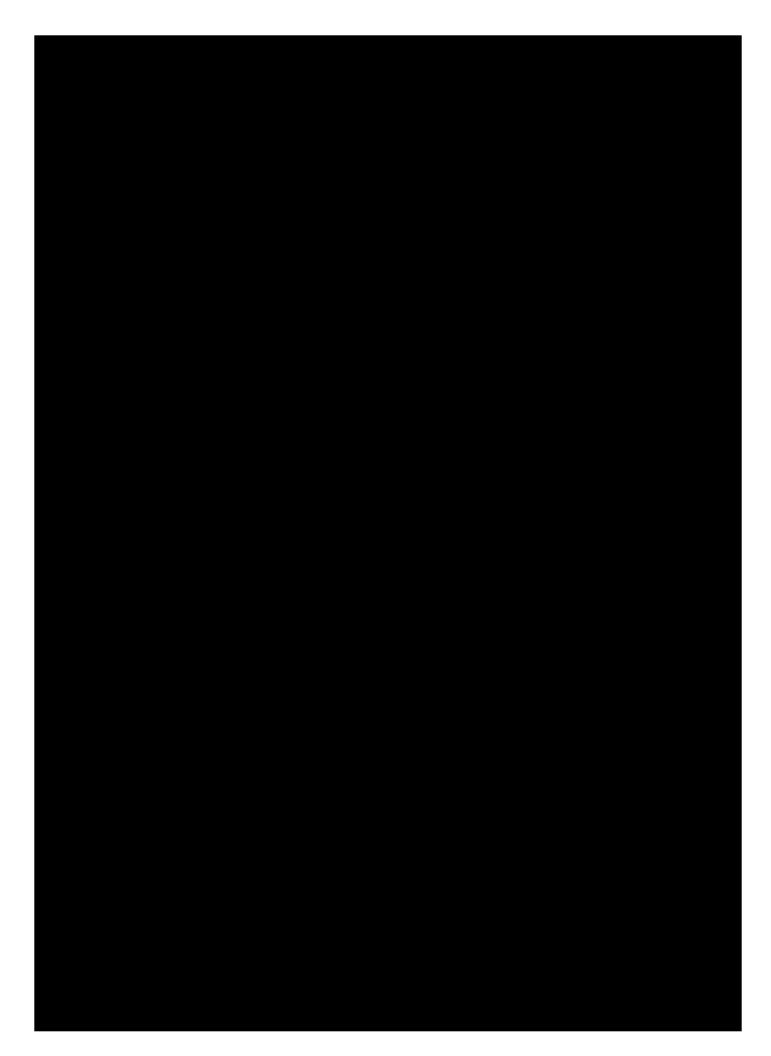




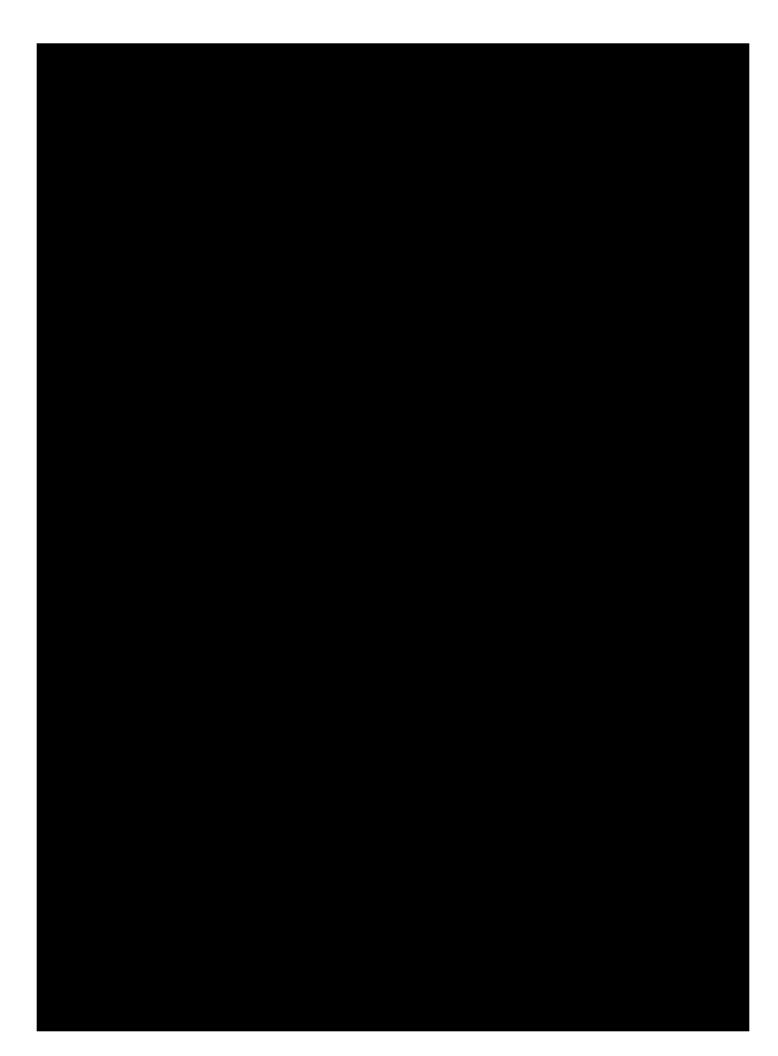




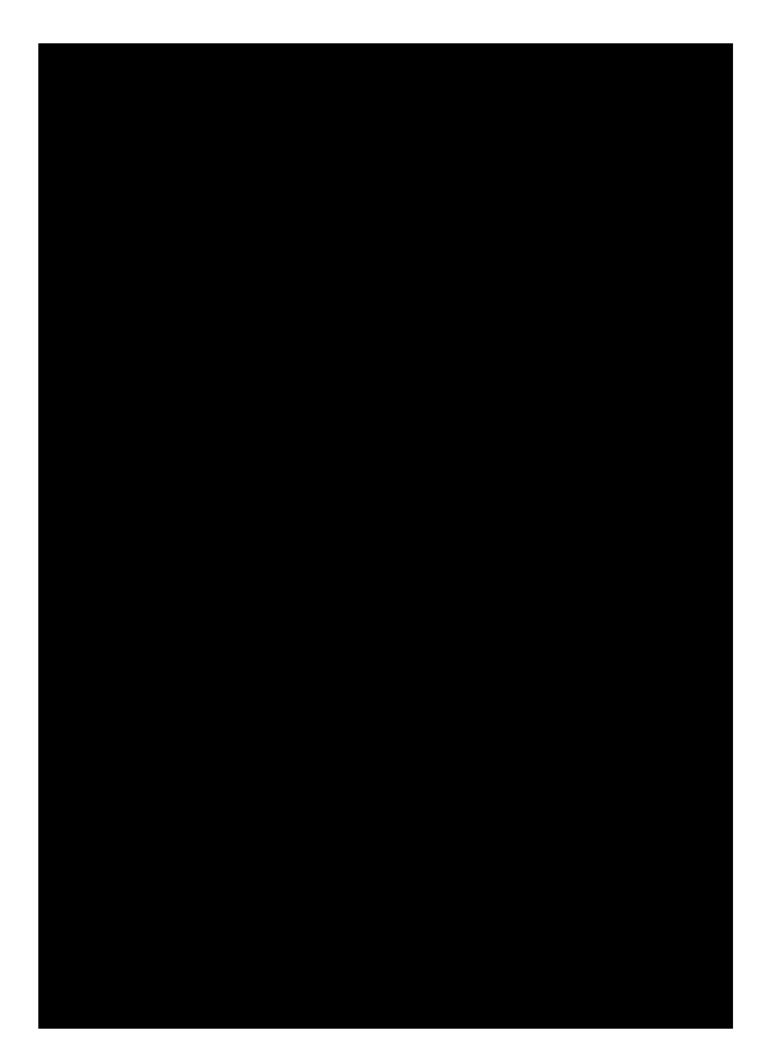


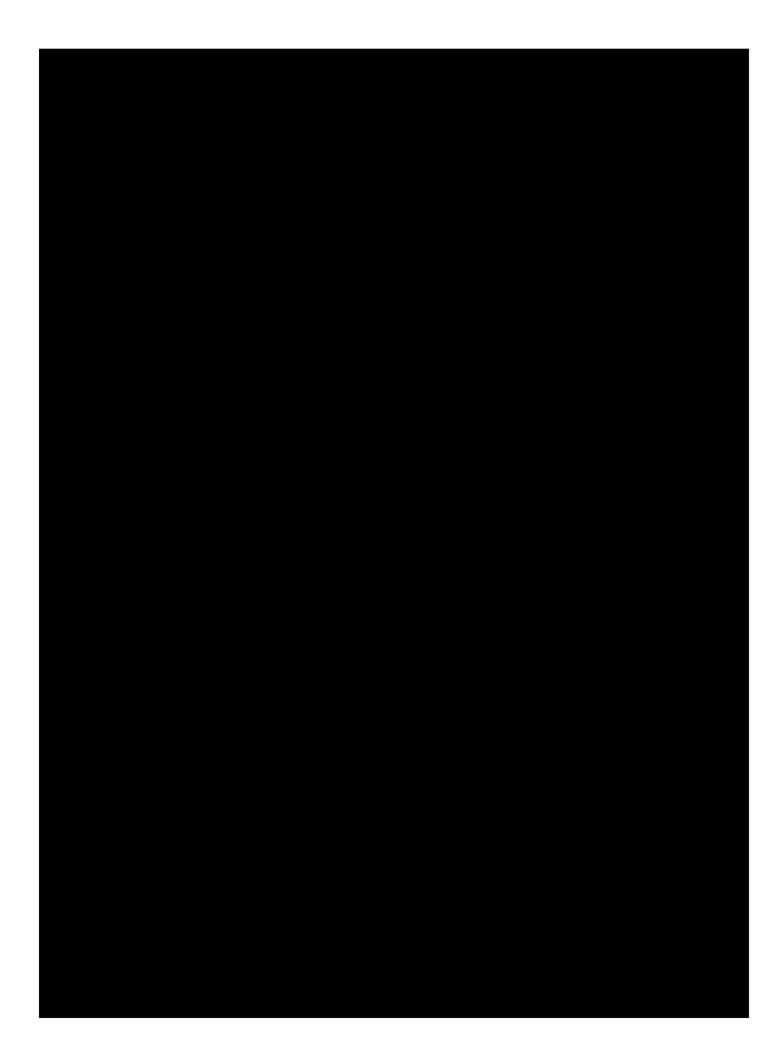
























Acceptance report

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Noise impact from the Ruland Road Station 2020				

Summary

This report provides the anticipated audible noise levels that will be generated by the operation of the proposed Ruland Rd (NY) converter station.

The Ruland Road converter station is located near the intersection of Ruland Road and Baylis Road in Melville, NY.

The converter station includes numerous equipment that generates audible noise. However, most of the electrical equipment is located inside the station buildings and, therefore, has little impact on the surroundings of the station.

There are four groups of outdoor equipment that generate audible noise in the proposed converter station:

- 1. Converter transformers with associated cooling fans;
- 2. Converter reactors:
- 3. Fans in the outdoor coolers used for cooling of indoor converter valves;
- 4. Climate control/HVAC equipment as well as the openings in the station buildings.

The sound calculations were based on typical sound power levels for all significant audible noise sources in the converter station.

The report also presents the sound requirements which the sound emitted by Ruland Rd HVDC station shall comply with.

Preliminary audible noise predictions of sound levels around the Ruland Rd converter station show that the facility will comply with the sound requirements.

This conclusion is illustrated by the results of computations presented in this report.





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1 General

The proposed Ruland Rd converter station on Long Island will be the onshore termination of a planned HVDC link for interconnection of offshore wind facilities.

The Ruland Road converter station is located near the intersection of Ruland Road and Baylis Road in Melville, NY.

The converter station includes numerous equipment that generates audible noise. However, most of the electrical equipment will be located inside the station buildings and, therefore, has little impact on the surroundings of the station. The main contributors to audible noise generated by the operation of the converter station will be equipment located outdoors.

1.1 Environmental Noise from the Industrial Plant

1.2 Environmental Noise Descriptors

Acoustical descriptors;

LAeq or LpA sound pressure levels in the report are relative to 20 μ PA and A-weighted

LwA sound power levels are relative to 1 pW and A-weighted.

Noise Maps with isophone-lines is an output from the preliminary Audible Noise Analysis, illustrating the combined sound pressure distribution in the topography from the contributing sound sources in the HVDC converter station.

1.3 Converter Station

The Ruland Rd converter station will include numerous equipment that generates audible noise.

In general, the main sound sources in the HVDC converter station are:

- Converter transformers;
- Cooling fans for converter transformer cooling plants;
- Converter valves located inside the valve halls (part of the converter building);
- Converter reactors located outdoors in the AC yard;
- DC filter equipment located in the converter building;
- Fans for valve cooling system;
- Climat control and HVAC equipment.

The most significant sources of noise impacting the surroundings of the station will be from equipment located outdoors.

There are four groups of outdoor equipment in the proposed HVDC converter station that will generate audible noise that may impact the surroundings of the installation.

That is:

- 1) Converter transformers (transformer enclosure) with associated cooling plant;
- 2) Fans in the outdoor coolers used for the cooling of the indoor converter valves;
- 3) AC filter components (reactors and capacitors);





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4) Auxiliary HVAC equipment and ventilation openings in the converter station buildings.

Most of the generated sound is within the frequency range of 100 to 2000 Hz.

2 Calculation Method Description

2.1 Prediction Methods

To verify compliance with the maximum specified sound levels at the immission points, a method of prediction of sound levels is required. In order to obtain the highest possible accuracy, it is necessary to use a 3D model of the converter station and its surrounding.

This has been done in the sound calculation program, SoundPLAN 7.4 of SoundPLAN GmbH. This calculation program is designed for sound calculations around industrial plants. Electrical substations and HVDC converter stations are examples of such systems.

The computation of audible sound around the Ruland Rd converter station has been done according to the calculation standard ISO9613-2:1996.

2.2 Environmental Parameters

Environmental parameters, such as temperature, relative humidity and air pressure are input parameters to calculate sound velocity and attenuation due to atmospheric absorption. The weather assumptions used for this study are part of the standard algorithm used.

2.3 Presentation of the Calculation Results

A way of presenting the calculation results is noise maps showing isophones-lines with constant noise level and with colored areas between them, which have been used in this report. The figures also show buildings and the different sound sources.

3 Noise Limiting Methods

The preliminary measures used for the Ruland Rd converter station are presented in Section 3.1.

3.1 Used Noise Limiting Measures

A list of preliminary external noise attenuation measures considered for the Ruland Rd converter station is given below:

- Converter transformer tanks will be enclosed in acoustical housings;
- Converter reactors will be acoustically optimized
- Cooling fans for valve cooling system will be of low noise type;
- Walls and roof of the station building will be acoustically optimized;
- Ventilation openings of the station building will be acoustically designed;
- A screening wall/station perimeter wall will be installed around the perimeter line of the station.

Use of noise mitigation measures will be evaluated during detailed design of the HVDC converter station. At that time, in order to meet the sound requirements, it





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may either be necessary to add noise mitigation measures or there may be a possibility to reduce one or more measures stated above.

4 Sound Propagation Calculations

In order to predict sound levels outside the Ruland Rd converter station, a preliminary sound propagation map for the station has been calculated.

The calculation has been carried out in a 3D (three-dimensional) model of the converter station and its closest surrounding.

The results of the calculations are described in Section 4.4.

4.1 Computation model

In order to predict sound pressure levels around the converter station, all significant sound sources in the station have been modeled.

The model assumes flat terrain around the converter station site. Therefore, elevation differences in the terrain and its influence on sound propagation have not been taken into account.

In the computations for the converter station, the typical sound power data for equivalent equipment for all significant sound sources, was used.

The sound sources are represented either as a point source or vertical line source or an area source in the model. This was determined based on the size and shape of the equipment.

4.1.1 Power load level

Maximum power level for the converter station has been used for noise calculations.

4.2 Audible Sound Level Limits

This section provides sound level requirements for the Ruland Rd converter station:

- As previously communicated for the site, the noise at any point on the converter station site property line, continuous airborne sound level shall not exceed 50 dBA.
- According to available data, maximum permissible sound-pressure levels at specified points of measurement (sensitive receptors) for noise radiated continuously from an establishment, between the hours of 10:00 p.m. and 7:00 a.m. shall be as shown in Table 1 below.

It is understood that these values are required by the Town of Huntington if they will be present in normally/presently used octave band system.

Octave band	63Hz	125Hz	250Hz	500Hz	1 kHz	2 kHz	4 kHz	8 kHz
Requirement	65 dB	53 dB	45 dB	40 dB	36 dB	33 dB	30 dB	27 dB

Table 1- Sound pressure level requirements of the town of Huntington

 The continuous airborne sound level with the Ruland Road converter stations operating at maximum power load, measured at each of the residential receptors shall not exceed 45 dBA.

This requirement may be problematic to verify due to fact that a normal night level of background noise in the area is possibly always higher than 45 dBA.





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4.3 Input Data

4.3.1 Layout

The preliminary station layout was used in developing the model for the Ruland Rd converter station.

The top view of the converter station is presented in the figure below.

4.3.1.1 Ruland Rd station

The acoustic model of the Ruland Rd station includes significant sound sources in the converter station, which are listed below:

- Three converter transformers with acoustical enclosures
- Cooling fans of converter transformers
- Cooling fans of valve cooling system
- AC filter equipment including reactors and capacitors
- Ventilation equipment in the station buildings

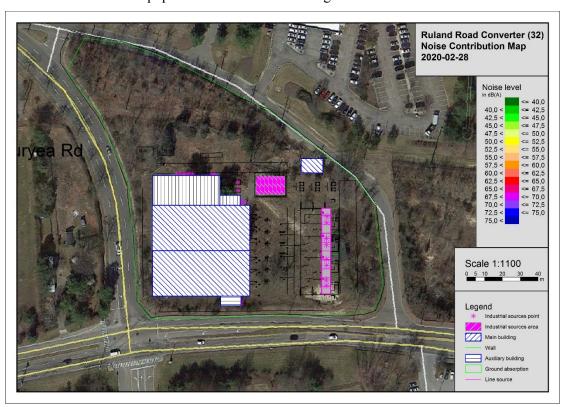


Figure 1– Ruland Rd converter station, location of the buildings and main equipment.

4.4 Results

The result shows preliminary predicted noise contribution from the typical sources within the converter station only. The result is valid for full capacity operation at nighttime.

4.4.1 Property line

The preliminary predicted noise contribution map (sound pressure levels caused by the equipment in the converter station) for the Ruland Rd station and the vicinity of





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this converter station is in the map below, shown in the aerial picture of the station area.

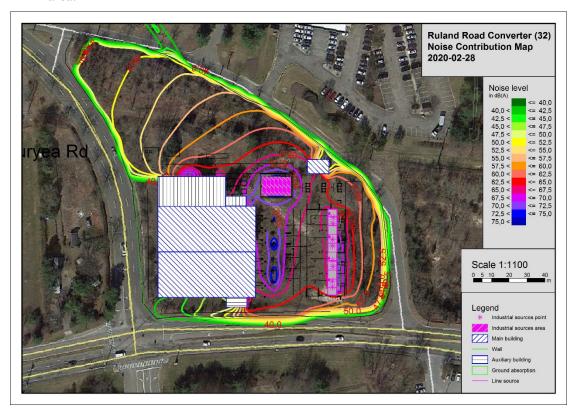


Figure 2 -Noise contribution map for the Ruland Rd station just outside the station, with station wall 10 feet high around.

The outdoor equipment in the converter station are the major contributors to noise from the station. Most of the electrical equipment sources for noise are totally enclosed in the station buildings and, therefore, well screened. That is, indoor equipment does not contribute significantly to noise level outdoors.

Due to short distances from the equipment to the property line, preliminary calculations show that a station wall will be required to limit the noise level at the station boundary.

The results of computations of sound propagation show that the Ruland Rd converter station will comply with the sound limits mentioned in Section 4.2 above. The noise level from the station will be below 50 dBA around the perimeter fence.





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4.4.2 Noise contribution in the area

The preliminary predicted noise contribution map for the area around the Ruland Rd station, showing noise contribution at longer distances from the station, is presented below.

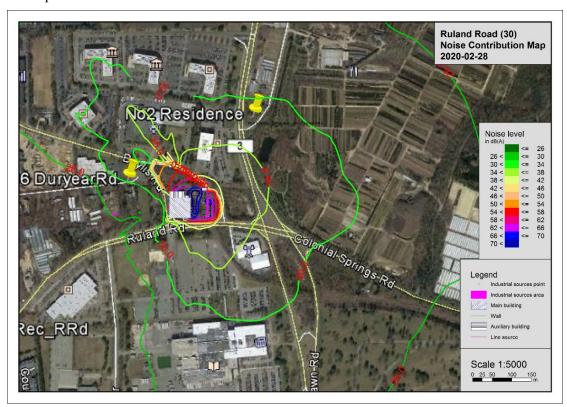


Figure 3– Noise contribution map for the Ruland Rd station on the aerial photo of the station area, at 2m above the ground.

The highest noise impact is caused in eastern direction from the converter. It is mainly caused by the cooling fans of the valve cooling system and the cooling fans associated with the converter transformers. These sources generate a broad-banded sound, which is typically not disturbing.

In western direction, the noise impact from the converter station will be the lowest.

4.5 Conclusion

Preliminary audible noise predictions of sound levels around the Ruland Rd converter station show that the facility will comply with the noise requirements as stated in Section 4.2.

The results are valid for the proposed layout and noise attenuation measures used for the equipment included in the converter station. The detailed noise study for the Ruland Rd converter station will be done during the detailed design phase of the project.



Acceptance report



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5 References

- [1] "Attenuation of sound during propagation outdoors". Part 2:

 A general method of calculation, ISO/DIS 9613-2, dated April 1996.
- [2] CIGRÉ Technical Brochure No 202, "HVDC Stations Audible Noise", working group 14.26, dated April 2002.

6 Revision history

Rev.	Prepared	Approved
Revisio	n text	





environmental consulting & engineering services

September 17, 2019

Howard Kosel Anbaric Development Partners 401 Edgewater Place, Suite 680 Wakefield, Massachusetts 01880

Re: Anbaric Development Partners – Baseline Sound Survey

South Brunswick, New Jersey ESS Project No. A592-003.16

Dear Mr. Kosel,

The following report summarizes the results of the Baseline Sound Survey (Sound Survey) completed by ESS Group, Inc. (ESS) on August 30, 2019 and provides a comparison of the combined sound levels from the measured baseline readings and ABB's predicted Project sound level contributions¹ at each location to the applicable permissible sound levels adopted by South Brunswick. The purpose of this Sound Survey was to establish the existing sound levels along the property line of the proposed Davidson Mill Road Converter Station (the "Project"); therefore, providing a baseline to determine whether the predicted sound levels from the proposed Project could potentially cause an exceedance of the permissible sound levels in the area surrounding the Project.

The results of the Sound Survey demonstrate that the predicted sound levels from the Project, when combined with the existing baseline sound levels, will comply with the maximum permissible sound levels specified in the New Jersey Noise Control Regulations (N.J.A.C 7-29) and the South Brunswick Code of Ordinances (Chapter 42 –Environment, Article IV – Noise Control). The sound levels during operation will be below 50 dB(A) (*Permissible A-Weighted Sound Level for Residential Properties*) along the property line associated with the residential property along Magee Lane. At all other locations, the sound levels during operation will be below 65 dB(A) (*Permissible A-Weighted Sound Level for Non-residential Properties*).

FACILITY SETTING

The proposed Davidson Mill Road Converter Station will be located in the Township of South Brunswick, New Jersey (see Attached Figure 1). The site is bordered by an overhead electric transmission line to the west, Davidson's Mill Road to the north, Deans Substation to the east, and an overhead electric transmission line to the south.

CONCEPTS OF ENVIRONMENTAL SOUND

Sound is generated by a variety of sources (e.g., a musical instrument, a voice speaking, or an airplane that passes overhead). Energy is required to produce sound, and this sound energy is transmitted through the air in the form of sound waves – tiny, quick oscillations of pressure just above and just below atmospheric pressure. These oscillations, or sound pressures, impinge on the ear, creating the sound we hear. The range of sound pressures that can be detected by a person with normal hearing is very wide,

¹ ABB, Predicted Audible Sound for Davidsons Mill Road Station, (Raleigh, North Carolina, 2019)









ranging from about 20 micro-pascals (μ Pa) for very faint sounds, at the threshold of hearing, to nearly 10 million μ Pa for extremely loud sounds, such as a jet during take-off at a distance of 300 feet.

Sound levels are reported using "sound pressure levels," which are expressed in terms of decibels, because the range of human hearing is so wide. The sound pressure level in decibels is the logarithm of the ratio of the sound pressure of the source to the reference sound pressure of 20 μ Pa, multiplied by 20.

The table below provides some examples of common sources of sound and their sound pressure levels. All of the sound levels presented in this report are provided in A-weighted decibels, abbreviated "dB(A)" or "dBA." The A-weighted sound level reflects how the human ear responds to sound, by deemphasizing sounds that occur in frequencies that the human ear is least sensitive to sound (at frequencies below about 100 hertz and above 10,000 hertz) and emphasizing sounds that occur in frequencies at which the human ear is most sensitive to sound (in the mid-frequency range from about 200 to 8,000 hertz). In the context of environmental sound, noise is defined as "unwanted sound."

Examples of Common Indoor and Outdoor A-weighted Sound Pressure Levels

Sound Level dB(A)	Common Indoor Sounds	Common Outdoor Sounds
110	Rock Band	Jet Takeoff at 1000 feet
100	Inside NYC Subway Train	Chain Saw at 3 feet
90	Food Blender at 3 feet	Impact Hammer (Hoe Ram) at 50 feet
80	Garbage Disposal at 3 feet	Diesel Truck at 50 feet
70	Vacuum Cleaner at 10 feet	Lawn Mower at 100 feet
60	Normal Speech at 3 feet	Auto (40 mph) at 100 feet
50	Dishwasher in Next Room	Busy Suburban Area at night
40	Empty Conference Room	Quiet Suburban Area at night
25	Empty Concert Hall	Rural Area at night

It is often necessary to combine the sound pressure levels from one or more sources. Because decibels are logarithmic quantities, it is not possible to simply add the values of the sound pressure levels together. For example, if two sound sources each produce 70 dB and they are operated together, they produce only 73 dB – not 140 dB as might be expected. Four equal sources operating simultaneously result in a total sound pressure level of 76 dB. In fact, for every doubling of the number of equal sources, the sound pressure level goes up another three decibels.

Sound frequencies are grouped in octaves. An octave band is defined as the range of frequencies from one frequency to double that frequency. Typically, environmental noise studies focus on the nine most commonly heard octave bands between 31.5 Hz (low bass, like a pipe organ) up to 8,000 Hz (high treble, like a flute).

Noise guidelines typically reference the L_{eq} . The L_{eq} is defined as the equivalent continuous sound pressure level. It represents the average sound level at a location that incorporates the sound pressure levels at the individual octave bands, and the variations in sound pressure levels over time. The L_{eq} is considered the









most representative indicator of the average sound pressure level at any given location over any time period.

APPLICABLE NOISE STANDARDS

Applicable noise standards for the proposed Project are contained within the New Jersey Noise Control Regulations (N.J.A.C 7-29) and the South Brunswick Code of Ordinances (Chapter 42 –Environment, Article IV – Noise Control) and are as follows:

Section 42-142 (a) of South Brunswick's noise ordinance states that "No person shall cause, suffer, allow, or permit the operation of any source of sound on any source property listed in section 42-138(a) in such a manner as to create a sound level that equals or exceeds the sound level limits set forth in Tables I, II or III (of the ordinance) when measured at or within the real property line of any of the receiving properties listed in Tables I, II or III (of the ordinance) except as specified in section 42-141(b)."

Please see attachment to view Tables I, II, and III.

BASELINE SOUND SURVEY METHODOLOGY

ESS collected sound level measurements at ten locations along the property line of the proposed Project based on the preliminary predictions of audible sound levels around the proposed Davidson Mill Road Converter Station (ABB, 2019), using precision integrating sound level meters that meet the requirements of American National Standards Institute (ANSI) Standards for Type I instruments. The sound level meter microphones were each fitted with a windscreen and then set up on a tripod at a height of five feet above ground. The sound level meters were calibrated at the beginning of each measurement period using acoustic calibrators following procedures pursuant to the National Institute of Standards and Technology (NIST). The sound level meters were programmed to sample and store A-weighted sound level data; including equivalent sound levels (Leq) and sound pressure levels (dBA) in each of the nine octave bands (Table 1).

Short-term measurements of 30 minutes were made at each of the locations between the hours of 12:00 PM and 6:00 AM on August 29, 2019. The measurement locations are described below (Figure 1):

- Site 1; along the southeastern property line of Lot 7 (non-residential)
- Site 2: along the northwestern property line of Lot 7 (non-residential)
- Site 3: along the southwestern property line of Lot 7 (non-residential)
- Site 4: at the southernmost corner of lot 12, the location closest to the existing Deans Substation (non-residential)
- Site 5: along the southwestern property line of lot 12 (non-residential)
- Site 6: along the northeastern property line of Lot 12 (non-residential)
- Site 7: along the northwestern property line of Lot 12, abutting Magee Lane and Lot 11 (adjacent to a residential property)
- Site 8: along the northern property line of Lot 12, abutting Davidsons Mill Road (non-residential)





- Site 9: along the northwestern property line of Lot 9, abutting the Right-of-Way (non-residential)
- Site 10: along the northernmost corner of Lot 9, abutting Davidsons Mill Road (non-residential)

SOUND SURVEY RESULTS

The results of the sound survey are summarized below (Table 1). This table presents the weighted average of the sound pressure level measurements taken at each of the ten locations, the predicted audible sound levels generated by the proposed Davidson Mill Road converter station, and the combined sound levels from the measured baseline readings and the predicted audible sound levels at each location according to ABB (2019). The table also compares the combined sound levels to the applicable permissible sound levels from Table I and III of Section 42-142 of the Town of South Brunswick's Noise Ordinance.

Table 1. Sound Pressure Level Measurements

		Site	1	2	3	4	5	6	7	8	9	10
F	NR	NR	NR	NR	NR	NR	R	NR	NR	NR		
Octave Band Sound Pressure Levels, dB												
Octave Band Center Frequency, Hz	Residential Limit ¹	Non- Residential Limit ¹				Base	eline Mea	surement	s, dB			
31.5	86	96	11.7	12.0	12.3	12.4	13.0	13.5	14.1	15.3	16.0	15.7
63	71	82	26.1	24.2	24.0	26.8	28.0	26.6	27.4	29.1	27.6	29.5
125	61	74	35.0	28.1	27.1	45.7	39.7	33.2	31.1	32.8	31.9	34.6
250	53	67	32.8	32.8	29.8	37.0	31.3	35.7	30.4	36.7	31.3	41.6
500	48	63	35.7	35.7	33.4	37.4	36.0	35.6	36.6	45.9	34.9	46.8
1000	45	60	34.7	35.6	29.1	29.7	28.9	30.4	37.4	51.8	35.3	54.0
2000	42	57	42.8	39.6	39.2	45.9	42.2	42.3	37.3	48.0	37.4	51.6
4000	40	55	51.6	50.2	44.4	41.3	38.2	37.5	39.1	41.7	51.2	51.0
8000	38	53	34.9	33.0	24.4	23.1	19.3	24.0	20.0	28.0	34.6	36.0
	Residential Limit ²	Non- Residential Limit ²	Baseline Measurement									
Leq (dB(A))	50	65	52.5	51.0	46.1	50.1	46.0	45.3	44.3	54.4	51.8	57.7
Predicted Project Operational Sound Contribution ³			57.5	55.0	52.5	55.0	57.5	52.5	35.0	35.0	40.0	35.0
	Combined	Sound Level ⁴	58.7	56.5	53.4	56.2	57.8	53.3	44.8	54.5	52.1	57.7

^{*}Receiving Property Categories

¹⁾ South Brunswick Code of Ordinances (Chapter 42 –Environment, Article IV – Noise Control): Table III. Maximum Permissible Octave Band Sound Pressure Levels in Decibels when measured outdoors



NR = Commercial facility, public service facility, non-residential portion of a multi-use property, or community service facility.

R = Residential Property, or residential portion of a multi-use property.



- South Brunswick Code of Ordinances (Chapter 42 Environment, Article IV Noise Control): Table II Maximum Permissible A-Weighted Sound Levels when measured outdoors
- 3) Predicted audible sound for Davidsons Mill Road Station (ABB, 2019) - Figure 3
- Sum of the Predicted Project Operational Sound Contribution and the August 30, 2019 Baseline Measurements $L_{\Sigma} = 10 \cdot \log_{10} \left(10^{\frac{L_1}{10}} + 10^{\frac{L_2}{10}} + \dots + 10^{\frac{L_n}{10}} \right) dB$

The results of the sound measurements taken at Sites 1 through 6 and Sites 8 through 10, combined with the applicable predicted sound level contribution from the proposed Project, demonstrate that the sound pressure levels will fall below South Brunswick's Maximum Permissible A-Weighted Sound Levels limits for non-residential properties during operation.

The results of the sound measurements taken at Site 7, combined with the applicable predicted sound level contribution from the proposed Project, demonstrate that the sound pressure levels will fall below South Brunswick's Maximum Permissible A-Weighted Sound Levels limits for residential properties during operation.

CONCLUSION

The results of the Sound Survey conducted at the proposed Davidsons Mill Road converter station site demonstrate that the Project will comply with the South Brunswick Code of Ordinances (Chapter 42 -Environment, Article IV – Noise Control). Should you have any questions or require any additional technical information, please do not hesitate to contact me at telephone number (781) 419-7749 or via email at mfeinblatt@essgroup.com.

Sincerely,

ESS GROUP, INC.

Michael E. Feinblatt Vice President

Environmental Compliance & Monitoring Services

Attachments

Figure 1 – Baseline Sound Survey

Chapter 42, Article IV, Section 42-142 – Maximum permissible sound levels (South Brunswick, New Jersey)











Anbaric Development Partners

South Brunswick, New Jersey

1 inch = 200 feet

Source: 1) NJOIT, Orthophotography, 2012 - 2013 2) Middlesex County Department of Planning 3) ESS Group, 2019

Legend

Project Property Boundary

Middlesex County Parcel Data



Baseline Sound Survey

Sec. 42-142. - Maximum permissible sound levels.

- (a) No person shall cause, suffer, allow, or permit the operation of any source of sound on any source property listed in section 42-138(a) in such a manner as to create a sound level that equals or exceeds the sound level limits set forth in Tables I, II or III when measured at or within the real property line of any of the receiving properties listed in Tables I, II or III except as specified in section 42-141(b).
- (b) Impulsive sound . Between 7:00 a.m. and 10:00 p.m., impulsive sound shall not equal or exceed 80 decibels. Between 10:00 p.m. and 7:00 a.m., impulsive sound which occurs less than four times in any one hour shall not equal or exceed 80 decibels. Impulsive sound which repeats four or more times in any one hour shall be measured as continuous sound and shall meet the requirements as shown in Tables I and II.

TABLE I. MAXIMUM PERMISSIBLE A-WEIGHTED SOUND LEVELS WHEN MEASURED OUTDOORS

RECEIVING PROPERTY CATEGORY	Residential property, or residential portion of a multi-use property		residential portion of a multi-use		Commercial facility, public service facility, non-residential portion of a multi-use property, or community service facility
TIME	TIME 7 a.m.—10 10 p.m—7 p.m. a.m.		24 hours		
Maximum A-Weighted sound level standard, dB	65 50		65		

TABLE II. MAXIMUM PERMISSIBLE A-WEIGHTED SOUND LEVELS WHEN MEASURED INDOORS

RECEIVING PROPERTY CATEGORY	Residential preside	ential	Commercial facility or non-residential portion of a multi-use property
TIME	7 a.m.—10 10 p.m—7 p.m. a.m.		24 hours
Maximum A-Weighted sound level standard, dB	55	40	55

Note— Table II shall only apply when the source and the receptor are separated by a real property line and they also share a common or abutting wall, floor or ceiling, or are on the same parcel of property.

TABLE III. MAXIMUM PERMISSIBLE OCTAVE BAND SOUND PRESSURE LEVELS IN DECIBELS

Receiving Property Category	residential multi-use	residential portion of a multi-use property		property, or tion of a multi- ty INDOORS	Commercial facility, public service facility, nonresidential portion of a multi-use property, or community service facility OUTDOORS	Commercial facility or non-residential portion of a multi-use property INDOORS
Octave Band Center Frequency, Hz	Octave Ba Pressure	and Sound Level, dB	Octave Band Sound Pressure Level, dB		Octave Band Sound Pressure Level, dB	Octave Band Sound Pressure Level, dB
Time	7 a.m10 p.m.	10 p.m7 a.m.	7 a.m10p.m. 10p.m7a.m.		24 hours	24 hours
31.5	96	86	86 76		96	86
63	82	71	72	61	82	72
125	74	61	64	51	74	64
250	67	53	57	43	67	57
500	63	48	53	38	63	53
1,000	60	45	50	35	60	50
2,000	57	42	47 32		57	47
4,000	55	40	45 30		55	45
8,000	53	38	43 28		53	43